

MX SITING INVESTIGATION GEOTECHNICAL EVALUATION

AD A11 3000

VERIFICATION STUDY MULESHOE VALLEY, NEVADA VOLUME II - GEOTECHNICAL DATA

PREPARED FOR BALLISTIC MISSILE OFFICE (BMO) NORTON AIR FORCE BASE, CALIFORNIA



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MX SITING INVESTIGATION GEOTECHNICAL EVALUATION

VERIFICATION STUDY - MULESHOE VALLEY NEVADA

VOLUME II - GEOTECHNICAL DATA

Prepared for:

U.S. Department of the Air Force Ballistic Missile Office (BMO) Norton Air Force Base, California 92409

Prepared by:

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30 June, 1981

FOREWORD

This volume of geotechnical data was compiled for the Department of the Air Force, Ballistic Missile Office (BMO), in compliance with Contract No. F04704-80-C-0006, CDRL Item 004A6. It contains the field data and laboratory test results from the Verification investigation of Muleshoe Valley. A synthesis of these data are available in Volume I (E-TR-27-MS-I).

The data in each section of this volume are preceded by an explanation of the format and terms used in the compilation.

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II-1-1 Activity Location Map, Muleshoe Valley, Nevada

In Pocket at end of Section

1.0 ACTIVITY MAP AND GEOGRAPHIC COORDINATES

Explanation: Locations of all field activities are shown in Drawing II-1-1, Activity Location Map (in pocket). The geodetic and Universal Transverse Mercator (UTM) coordinates of all activities are listed in Table II-1-1.

```
MULEDHOS /AULEY ACTIVITY LOCATIONS
  40-
          5 8 0 D & T 10 0 0 0 0 P 0 .
                                   UTY 00040.
                                    20%E 12
        Des MIN DUS MIN
                                  N(KY) E(K4)
2041NS SITES
                                4243.94
MS- 601 38 22.14 114 44.97
                                           690.01
                                4231.11
        38 12.52 114 49.11
18 14.75 114 45.14
                                           590.99
CPT SITES
"S- CC1 C2 25.45 114 43.42
                                4255.14
                                           598.71
                                           597.37
         38 25.55 114 --.00
                                4255.30
         03 22.14 114 44.97
                                           633.51
                                 4248.94
78- 004 38 22.17 114 45.31
                                 4243.96
    003 0: 22.01 11. +3.<sub>25</sub>
73- 036 33 21.73 114 43.53
75- 037 36 18.33 114 42.55
                                 42-1.94
                                           578.73
Y0- 008 33 18.23 114 40.63
                                 42-1.85
MS- 009 38 13.15 114 44.65
                                 4241.53
MS- 010 38 18.03 114 45.66
MS- 011 33 13.57 114 51.6-
                                           005.70
                                 4141.41
                                 4232.87
                                 4231.21
    c12 38 12.97 114 50.12
                                 4235.35
   013 35 15.09 114 43.50
014 38 14.33 114 44.79
        38 14.75 114 45.34
                                 4005.00
    :1 :
        33 14.63 114 47.45
38 17.07 114 45.35
   01 c
   21 7
                                            594.54
                                 4239.51
                                 4239.79
MS- 018 38 17.24 114 47.51
            17.20 11- -1.21
    213
"3- 020
"3- 021
                                            591.54
         38 14.19 114 48.53
                                 4234.11
         28 14.34 114 49.05
                                 4033.30
                                            590.11
MS- 022 38 12.52 114 49.11
MS- 023 38 12.03 114 43.32
                                 4231.01
                                            590.99
                                 4230.07
                                            c92.35
MS- 024 33 11.55 114 47.69
                                 4229.27
GEOLOGIC STATIONS
MO-9801 38 10.00 114 50.01
                                 4231.87
                                           359.57
YS-GSC2 38 11.83 114 43.30
                                 4329.73
                                            592.00
MS-3803 38 21.59 114 47.83
                                 4243.33
                                            497.50
MS-3804 38 20.25 114 45.47
                                            695.95
                                 4245.43
MS-3500 38 22.16 11+ 45.71
                                 4248.75
                                            575.43
Y3-3806 38 10.39 114 +6.72
                                 4228.03
                                            59-.55
```



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GEODETIC AND UTM COORDINATES
OF ACTIVITY LOCATIONS
MULESHOE VALLEY, NEVADA
PAGE 1 OF 4

30 JUN 81

TABLE II-1-1

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E-TR-27-MS-II
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SECDETIC COGRO.
                                    UTM 00020.
  4 0 T
                                      10.E 12
                      L073.
        bes min bes min
                                  1.(37)
                                 4234.37
4236.33
M3-3307 38 14.32 114 48.51
43-3308 38
            15.24 114 49.15
                                            590.32
                                 4239.50
M S = 383 P
         35 17.15 11. 49.17
                                            593455
            17.13
                    114 +5.39
73-3310
                                 4234.71
                                            593.39
                                 4233.75
13-3311
            -15.61 114 44.25
                                 4233....
M3-3310 D8 13.24 114 44.00
M3-3310 B8 01.51 114 40.30
         38 13.2- 11- -4.00
                                            59:03
                                 4247.33
                                            591.J.
10-3314 38
            21.54 114 44.82
                                 4247.25
                                            t?t.36
YS-3815 38 24.42 114 43.04
                                            500.3
                                 4237.15
M8-3316 38 26.54 114 42.73
                                            600.57
45-3317
                                            : ?7.5.
         38 25.63 114 44.23
                                 4255.44
KS-3818 33
            23.11 11+ +3.38
                                 4254.4=
                                            £98.5
MS-SS19 33 22.25 114 44.52
                                 42-9.17
                                            590.30
ms-6520 38 20.78 114 40.00
                                 +250.19
"5-GS21 38 12.27 114 41.73
                                 -2-1.-4
18-4820 38 22.34 114 47.00
                                 4349.35
                                            593.51
MS-GS23 38 20.55 114 47.04
                                            593.57
                                 4245.93
                                 4245.37
73-3824 38 21.05 114 45.76
73-8825 33 21.73 114 42.32
                                 4243.29
                                 42+5.14
MS-G325 35 20.14 114 42.40
MS-G827 38 19.14 114 4-.14
                                 4243.43
Y3-3328 38 20.15 114 44.03
Y3-3829 38 20.01 114 45.34
                                 4045.05
                                            699.03
                                 4044.07
4020.98
4028.90
4009.84
4009.84
MS-3530 38 10.31 114 47.13
MG-0831 38 11.37 114 48.17
Y2-3832 38 11.35 114 47.+1
Y3-3833 38 11.69 114 47.19
Y0-3834 38 13.23 114 44.49
                                 +23+++7
                                            597.27
48-3335 3: 14.31 114 44.75
                    114 42.79
                                            700.10
"3-6036 33 15.32
                                 4256.41
M2-3527
M5-3528
         33 15.-3 114 42.93
                                 +235.61
                                            599.89
                                 4225.43
4225.43
4227.55
         38 10.20 114 52.43
                                            5 35 . I 5
             9.56 114 52.37
11.37 11.50.75
                                            535.53
M3-3839 32
48-6348
         35 11.37
                                            233.23
          :3 11.77 11→ 51.43
45-GS41
                                            537.5
Y3-93+2 03 13.90 11+ 52.30
Y3-3543 03 19.+2 114 47.30
                                            585.51
                                 4233.43
                                 4243.83
                                            693.29
Y3-3344 38 20.66 114 45.19
                                 4246.21
                                            596.35
MS-3845 38 17.53 114 45.17
                                 4240.33
                                            595.37
YE-3845 33 15.21 114 44.73
                                 4237.99
                                            597.15
                                            590.75
MS-5547 52 17.33 114 44.95
                                 4240.15
MG-35+8 38 12.51 114 48.93
                                 4231.00
                                            591.17
```

TOURSHOE NAUGON ACTIVITY LOCATIONS



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GEODETIC AND UTM COORDINATES
OF ACTIVITY LOCATIONS
MULESHOE VALLEY, NEVADA
PAGE 2 OF 4

30 JUN 81

TABLE 12-1-1

```
DEESHOE VALUEY ACTIVITY UNDATIONS
  307
          GEODETIC COORD.
                                  10.5 11
                     1043.
           N(KY) E(KY)
REFRACTION LINES
MS- 301 38 25.45 114 43.42
MS- 802 38 22.14 114 44.97
                                --255.14 595.71
"S- SC3
                                -1-1-1-
                                           545.51
/3- 503 38 18.30 11. +2.60

/3- 304 33 15.07 114 +7.50

/3- 305 38 11.55 114 +7.57
                                           700.13
                                -1-1.3-
                                120.27
                                           549.25
                                           593.13
                                           731.5
MG- 806 38 13.57
                   11- 51.1-
         38 25.12 114 42.12
43- 507
73- 338 38 11.71 114 43.3.
MS- 309 38 14.35 114 45.53
                                4127.14
                                           392.55
                                           5,45.43
                                +235.+5
43- 810 38 10.35 11- 45.37
                                4027,43
PESISTIVITY LINES
                                           372.71
700.13
MG- PG1 38 25.46 114 43.42
                               4255.14
MO- RO3 35 13.30 114 42.65
                               4241.94
MG- PC4 38 15.09 114 42.50
                                4235.95
                                           694.05
                                4229.27
                                           593.12
M3- 905 33 11.55 114 47.69
                                4232.87
MS- RO5 33 13.57 114 51.24
                                           537.35
730.53
YS- ROT 38 25.12 114 42.13
MS- RD8 38 11.71 114 43.00
MS- RD9 38 14.85 114 45.50
                                           593.55
                                           395.12
MS- R10 33 10.56 114 46.37 4227.43
                                           095.09
SURFICIAL SCIL SAMPLES
Y0-0305 38 02.01 11+ 43.30
                                4243.73
                                           590.25
#3-0908 38 13.23 114 43.32
#3-0910 23 18.08 114 45.66
                                4241.35
                                           691.73
                                           095.75
                                --2-1.-1
                                           529.50
vs-0812 38 12.97 114 50.18
                                4231.31
M3-0813 33 15.07 114 43.50
                                4235.95
                                           699.05
                                4234.11
45-0513 38 17.24 114 47.61
                                           592.93
MS-0820 39 14.19 114 48.63
                                           591.54
MS-0523 38 12.00 114 48.33
                               -230.07
                                           692.JE
TEST PITS
                                           597.37
MS- PC1 38 25.56 114 44.00
                                4255.30
                                4254.30
                                           700.32
M3- PC2 38 24.99 114 42.33
75- PO3 38 21.73 114 42.50
                                 4243.37
                                           700.25
MS- P34 33 13.15 114 44.55
                                 42-1.53
                                           697.25
```



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GEODETIC AND UTM COORDINATES
OF ACTIVITY LOCATIONS
MULESHOE VALLEY, NEVADA
PAGE 3 OF 4

30 JUN 81

TABLE T-1-1

MULESHOE VALLEY ACTIVITY LOCATIONS

ID.	GEODETI: LAT. DEG MIN	Long. Des vin	UTN 00 IONE N(KA)	12 1(<y)< th=""></y)<>
VG- PC6 MG- PC3	38 17.07 38 17.57 38 11.55	11+ 44.79 11+ +7+5 11+ +6.55 11+ 47.69 11+ 51.2+	4235.53 4214.91 4239.51 4229.27 4232.37	697.20 030.07 59.05 59.12 59.65
MG- TGG MG- TGG MG- TGG MG- TGG MG- TGG MG- TGG	33 25.40 38 22.17 30 22.1+ 33 13.30 33 14.75 36 12.52 38 14.04	114 +3.42 114 +0.21 114 44.97 114 +2.08 114 46.34 114 49.11 114 49.63 114 48.22	4255.14 4245.96 4245.94 4241.94 4235.23 4231.01 4233.30 4240.05	595.71 594.35 596.61 709.13 697.11 597.11 597.07
	ELL SITES	114 45.37	4241.41	595.19



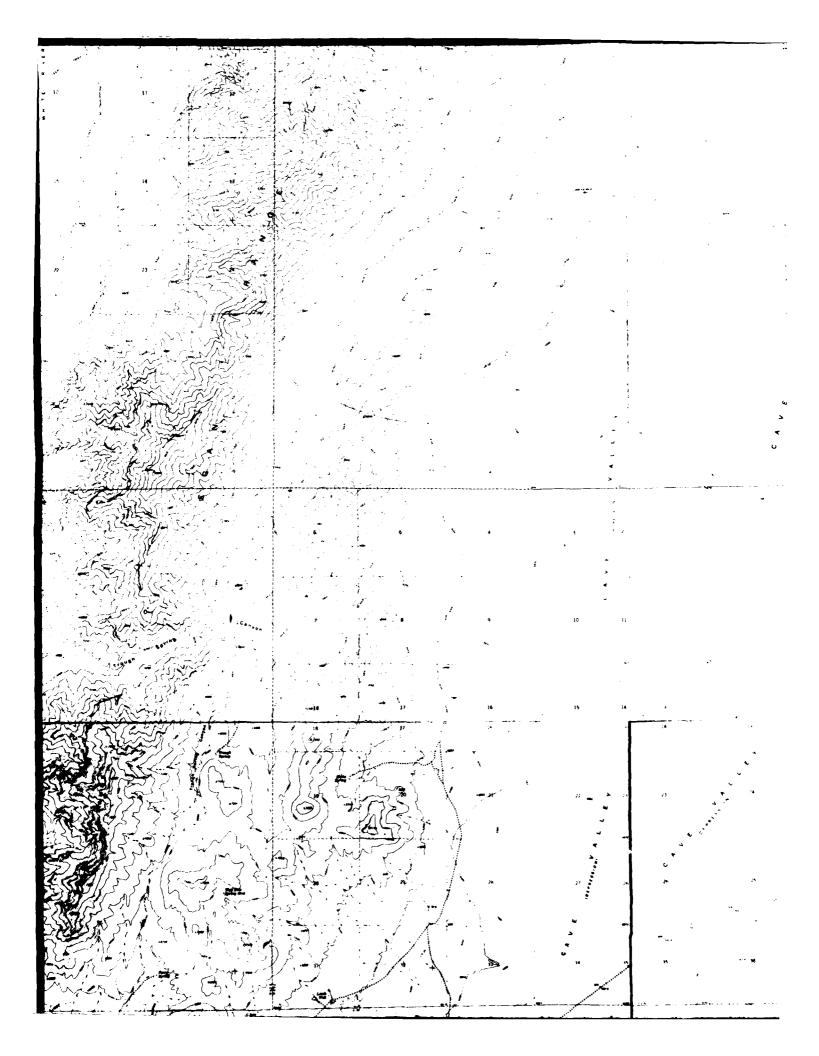
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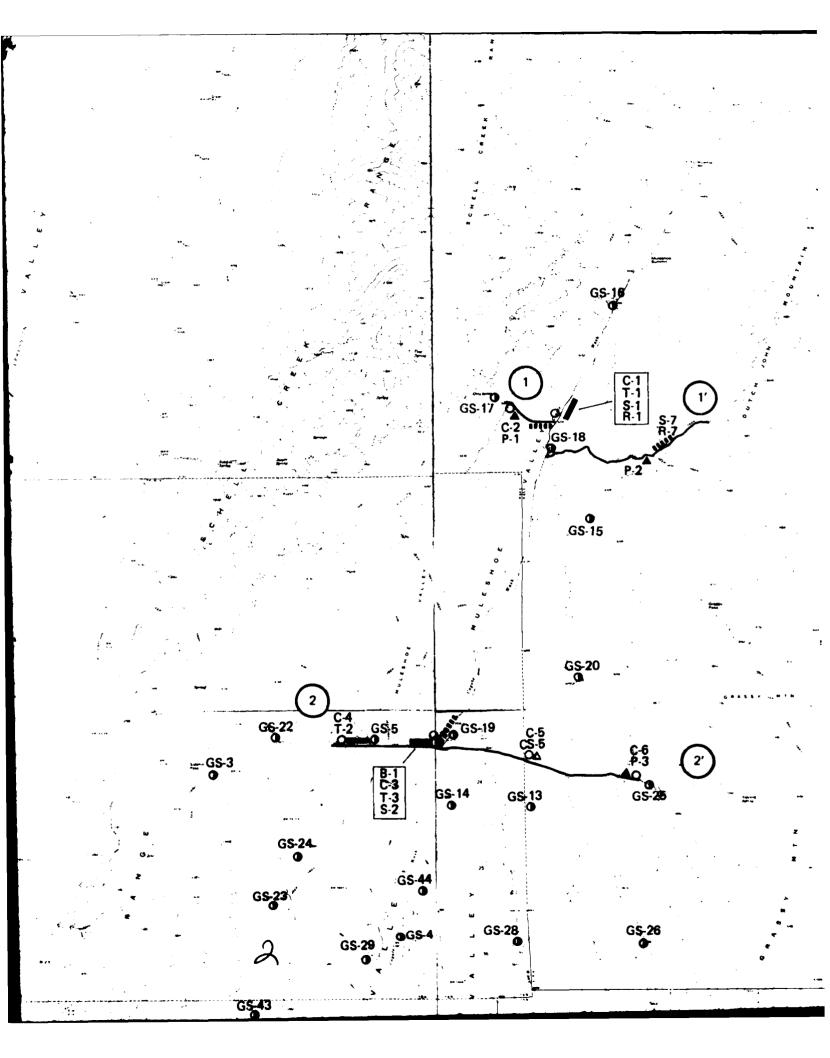
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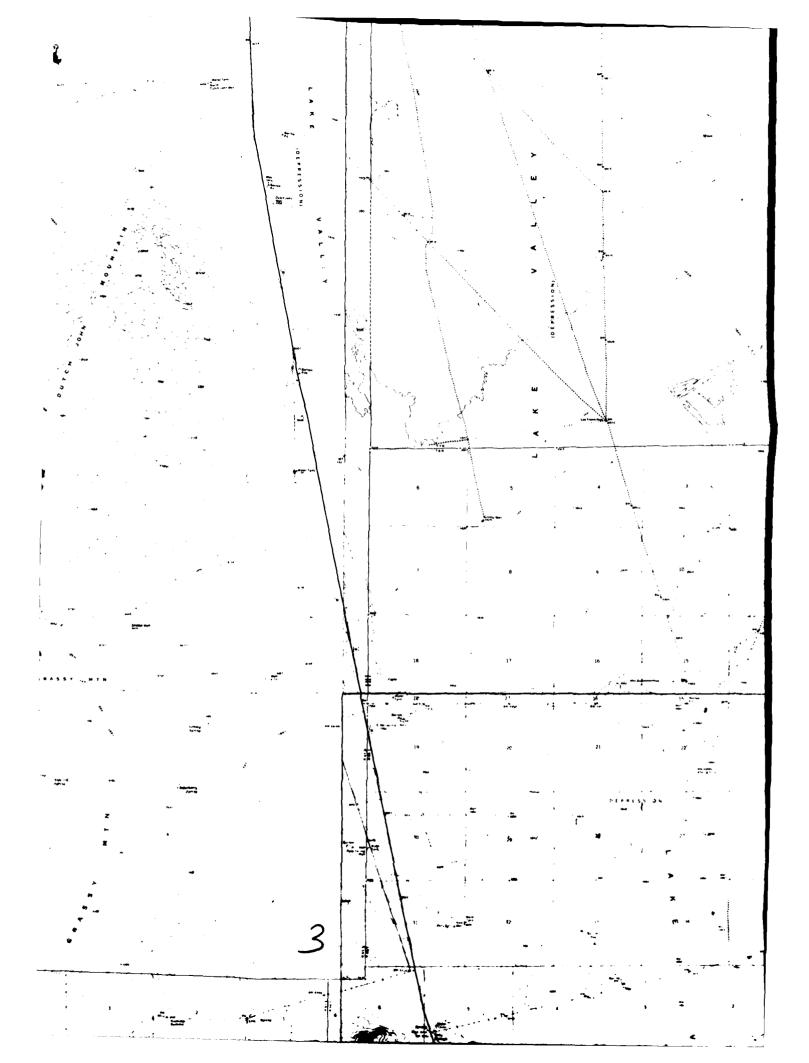
GEODETIC AND UTM COORDINATES
OF ACTIVITY LOCATIONS
MULESHOE VALLEY, NEVADA
PAGE 4 OF 4

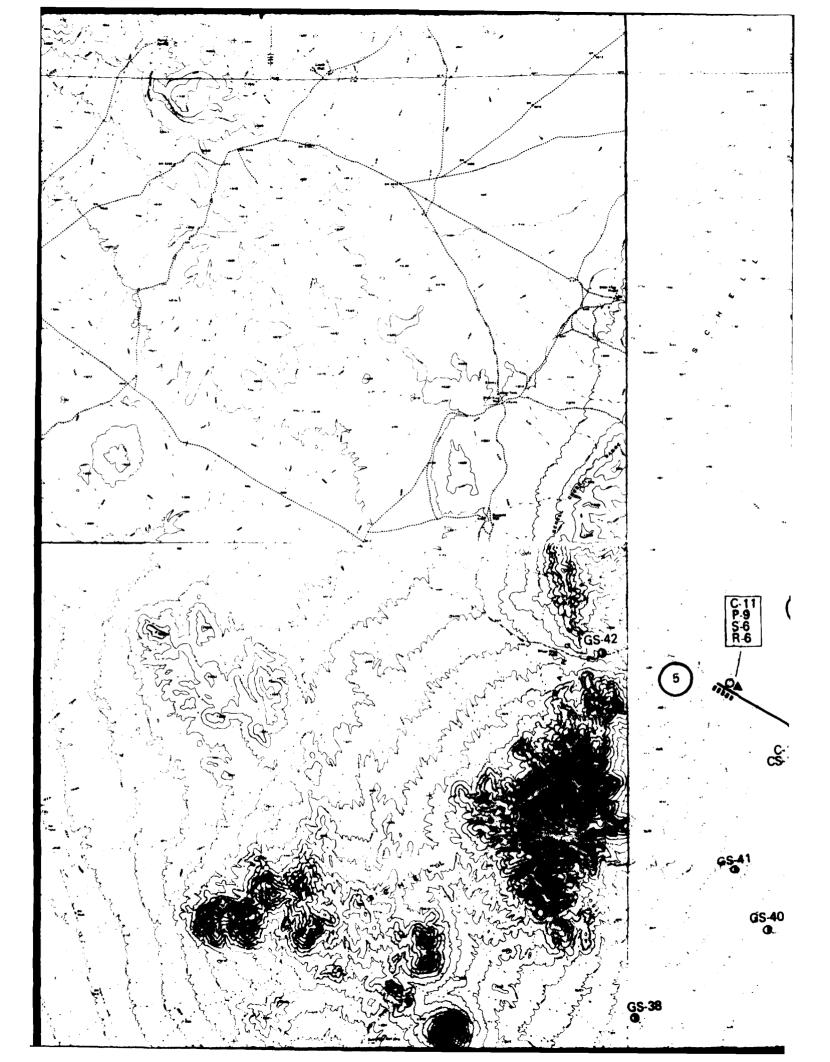
30 JUN 81

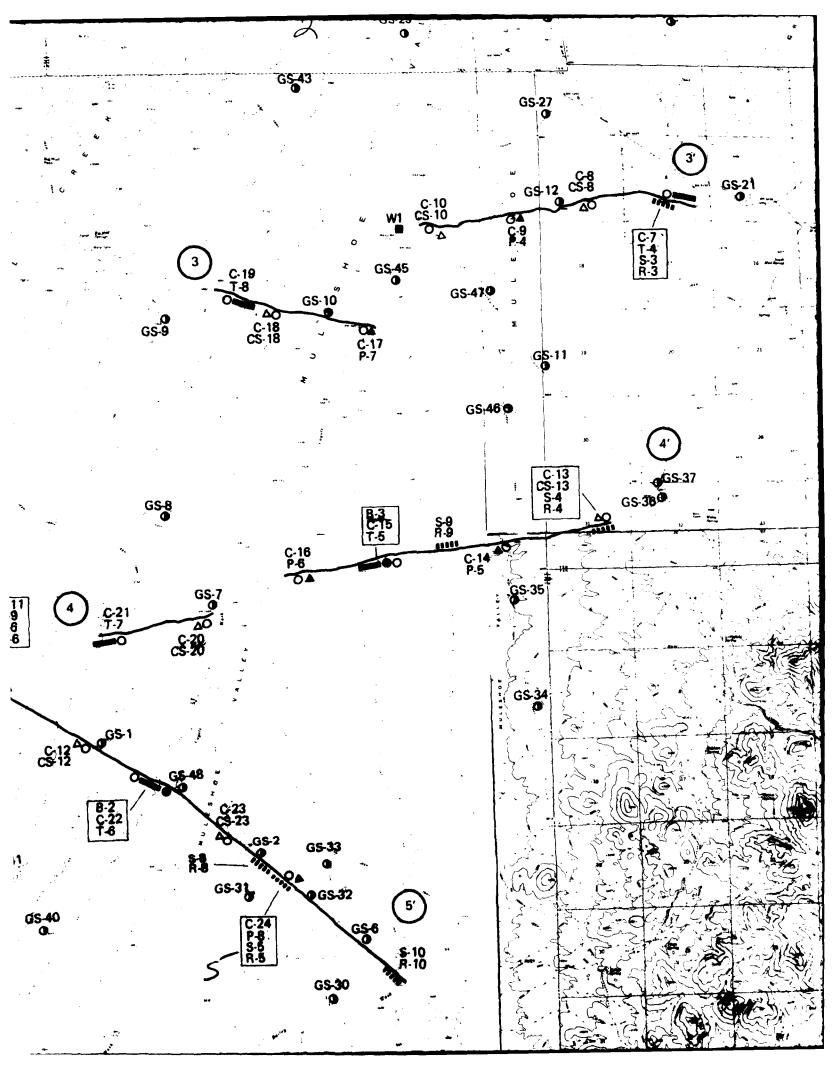
TABLE II-1-1

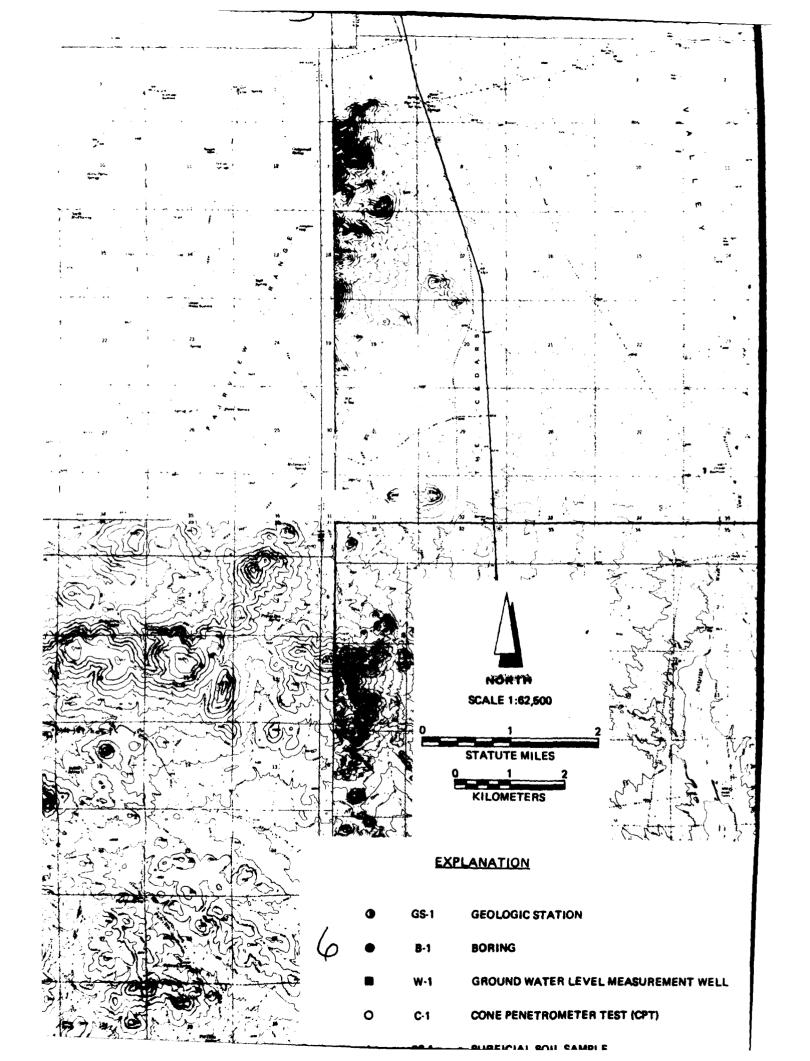


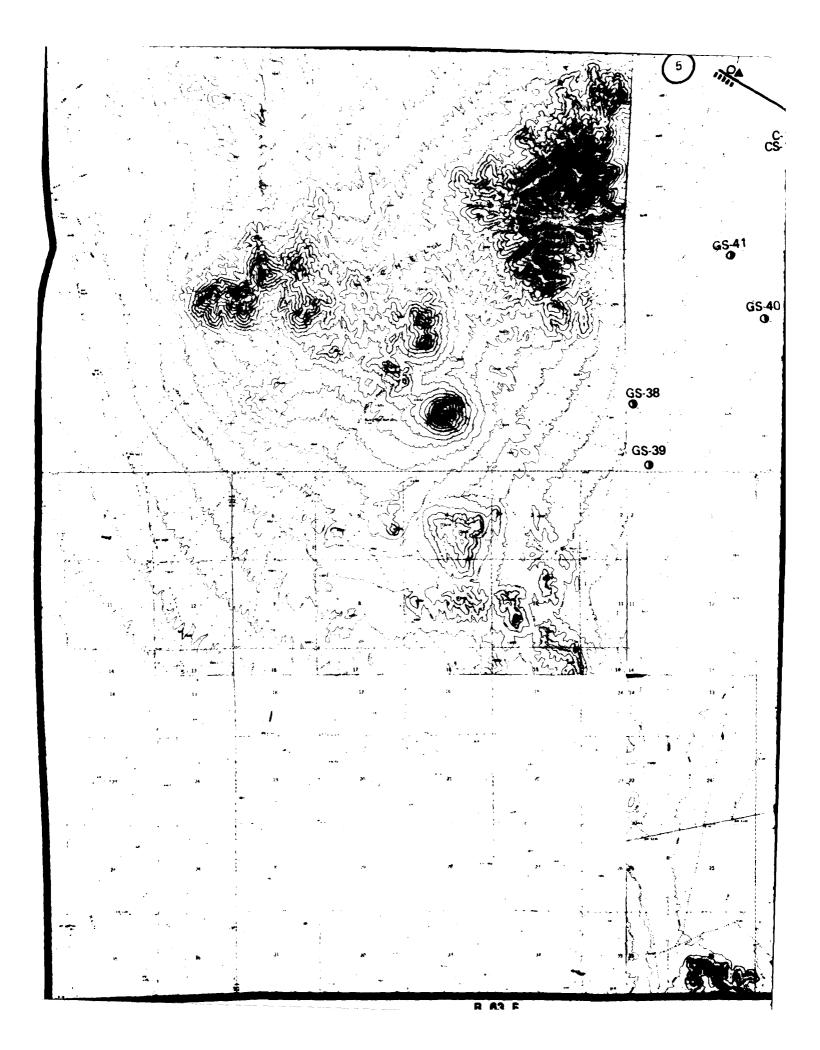


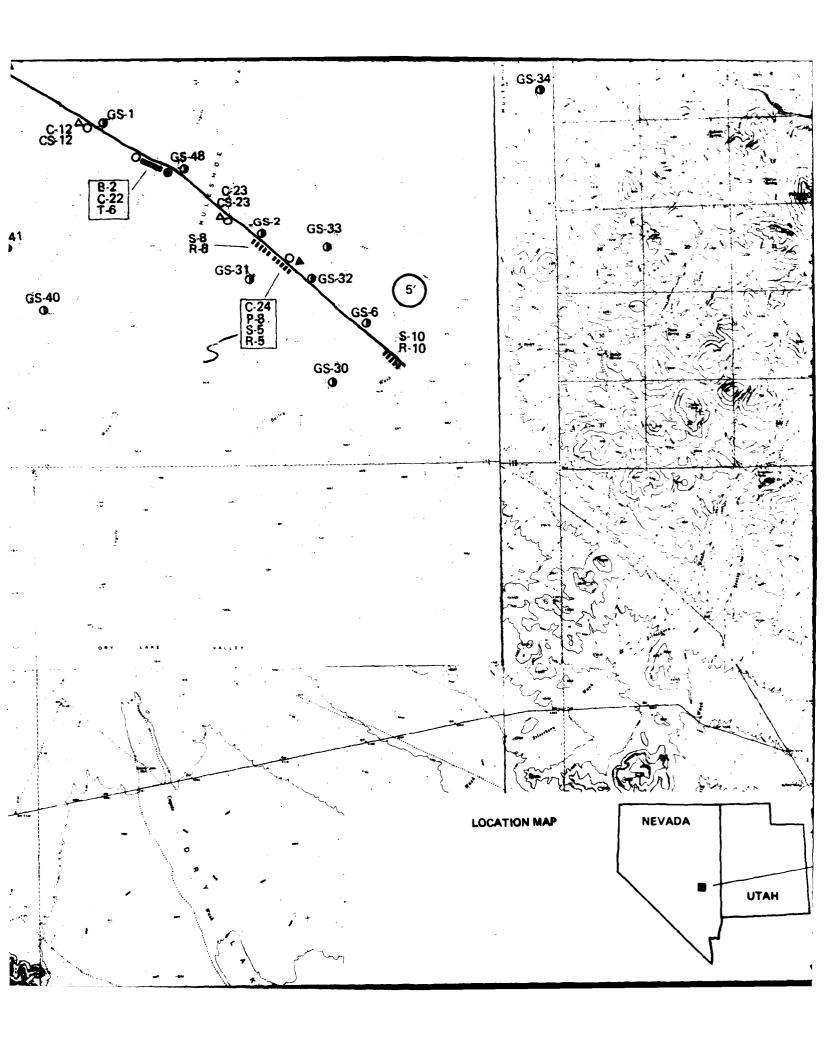




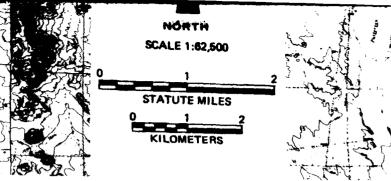












EXPLANATION

GS-1 GEOLOGIC STATION

● B-1 BORING

W-1 GROUND WATER LEVEL MEASUREMENT WELL

O C-1 CONE PENETROMETER TEST (CPT)

Δ CS-1 SURFICIAL SOIL SAMPLE

T-1 TRENCH

P-1 TEST PIT

S-1 SEISMIC REFRACTION LINE
R-1 ELECTRICAL RESISTIVITY LINE

1 ACTIVITY LINE

NOTE: Due to the exaggeration of the map symbols, the exact location of any combination of entities is where either the bering (1st) or the CPT (2nd) is diseased, Single settleties are most securely jocated assess the center of the symbols.

VERIFICATION STUDIES FY 80



MX SITING INVESTIGATION
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ACTIVITY LOCATION MAP
MULESHOE VALLEY, NEVADA

30 JUN 81

DRAWING II-1-1

2.0 GEOLOGIC STATION DATA

Explanation: Geologic stations were established at selected locations throughout the valley at which detailed descriptions of surficial basin-fill deposits or rock were recorded. All data taken on surficial basin-fill units at the geologic stations are listed in Table II-2-1, and an explanation of the column headings in the table is given below. An example of the field data sheet is shown on Figure II-2-1. At stations where rock descriptions were made, only geologic unit designations are listed. A general explanation of all geologic unit symbols used in Verification studies is included at the end of this section.

Column Heading Table II-2-2	Explanation
Station Number	Geologic stations are numbered sequentially. (e.g., NMSG001; N= Nevada-Utah Study Area; MS= Valley abbreviation [Muleshoe]; G= Geology Station).
Geol. Unit	Generalized mapped geomorphic unit (see explanation below). The grain-size designations (s, g, and f) indicate sand, gravel, and fines, respectively.
MPS (mm)	Average Maximum Particle Size in millimeters.
Grain Size (%B, %C, %G, %S, %F)	Estimated particle size distribution using the Unified Soil Classification System. Percentages of boulders (%B) and cobbles (%C) are based on the entire deposit, whereas percentages of gravel (%G), sand (%S), and fines (%F, are taken only on the fraction composed of particles less than 3 inches (76 mm) in diameter. Note: The symbol, Ø (occasional), indicates between one and five percent; zero indicates 0 to one percent.

Laboratory analyses of selected soil samples using the Unified Soil Classification System.

USCS Soil class according to the Unified Soil Class-ification System.

Munsell Color Soil color based on standard Munsell Soil Color Charts.

Source Rock Rock types of coarse clasts (gravel) listed in Types order of abundance.

Physical Data listed in columns 6 through 15 address specific soil properties. These are listed below in parentheses following the column heading number and are also listed at the bottom of Table II-2-1. Data are coded with each numerical entry referring to a specific soil condition as listed below.

- 6 (Grain Shape) 1) Angular, 2) Subangular, 3) Subrounded, 4) Rounded, 5) Well rounded
- 7 (Moisture 1) Dry, 2) Slightly Moist, 3) Moist, 4) Very Content) Moist, 5) Wet
- 8 (Plasticity 1) None, 2) Low, 3) Medium, 4) High
 of Fines)
- 9 (Consistency) Coarse grained: 1) Very Loose, 2) Loose, 3) Medium Dense, 4) Dense, 5) Very Dense Fine grained: 1)Soft, 2) Firm, 3) Stiff, 4) Hard
- 10 (Structure)
 1) Non-stratified, 2) Stratified, tabular,
 3) Stratified, other (lensed, cross bedded, discontinuous beds)
- 11 (Cementation- 1) None, 2) Weak, 3) Moderate, 4) Strong Induration)
- 12 (Depth to Depth to layer (in centimeters) exhibiting Cemented cementation-induration described in Column 11 (above)
- 13 (Weathering 1) Fresh, 2) Slight, 3) Moderate, 4) Very of clasts)

14 (Soil	1) None (A-C profile), 2) Poor	(incipient
Profile	B-horizon), 3) Well (prominant	B-horizon)
Development)		

15 (Caliche 1) None, 2) Stage I, 3) Stage II, 4) Stage Development) III, 5) Stage IV

Terrain Terrain information at the data location is broken into the following categories:

Drainage Depth Average depth of drainages (in feet) (ft)

Drainage Width Average width of drainages (in feet) (ft)

Slope (%) Average slope of ground surface (in percent grade)

Sample Number of samples taken

GENERALIZED GEOLOGIC UNITS

Explanation

Surficial Basin-fill Units

- Al Younger Fluvial Deposits Major recent stream channel and floodplain deposits.
- A2 Older Fluvial Deposits Older incised stream channel and floodplain deposits in elevated terraces bordering major recent drainages. Note: Not mapped in Muleshoe Valley.
- A3 Eolian Deposits Windblown deposits of sand occurring as either thin sheets (A3s) or dunes (A3d).
- A4 Playa and Lacustrine Deposits Deposits occurring in modern, active playas (A4) or in either inactive playas or older lake beds and abandoned shorelines associated with extinct lakes (A4o).
- A5 Alluvial Fan Deposits Alluvial deposits consisting of debris flow and water-laid alluvium near mountain fronts, grading into predominantly water-laid alluvium deposited in shifting distributary channels near the basin center. Younger (A5y), intermediate (A5i), and older (A5o) alluvial fans are differentiated by surface soil development, terrain conditions, and present depositional/erosional environment.

Grain sizes of these deposits (except A3 deposits, which are exclusively sandy) are indicated by a single letter (f, s, or g) following the geologic unit symbol. These letters indicate the predominant grain size and range of soil types according to the Unified Soil Classification System.

- f fine-grained clays and silts (ML, CL, MH, CH)
- s sands (SP, SW, SM, SC)
- g gravels (GP, GW, GM, GC)

ROCK UNITS

- I Igneous (undifferentiated). Rocks formed by solidification of a molten or partially molten mass.
 - Il Intrusive Plutonic rocks formed by solidification of molten material beneath the surface (e.g., granite, granodiorite, diorite, gabbro).
 - 12 Extrusive (intermediate and acidic) Volcanic rocks of intermediate and acidic compositon formed by solidification of molten material at or near the surface, (e.g., rhyolite, latite, dacite, andesite).
 - I3 Extrusive (basic) Volcanic rocks of basic composition, generally formed by solidification of molten materials at or near the surface (e.g., basalt).
 - I4 Extrusive (pyroclastic) Rocks formed by accumulation of volcanic ejecta (e.g., ash, tuff, welded tuff, agglomerate).
- S Sedimentary (undifferentiated) Rocks formed by accumulation of clastic solids, organic solids, and/or chemically precipitated minerals.
 - Sl Arenaceous and/or Siliceous Rocks Composed of sandsize particles (e.g., sandstone, orthoguartzite) or of cryptocrystalline silica (e.g., opal, chert).
 - S2 Carbonate Rocks Composed predominantly of calcium carbonate detritus or chemical precipitates (e.g., limestone, dolomite, chalk).

- S3 Argillaceous Rocks Composed of clay and silt-sized particles (e.g., siltstone, shale, claystone).
- S4 Evaporite Rocks Precipitated from solution as a result of evaporation (e.g., halite, gypsum, anhydrite, sylvite).
- S5 Coarse Clastic Rocks Composed of gravel sized or larger clasts (e.g., conglomerate, breccia).
- M Metamorphic (undifferentiated) Rocks formed through recrystallization in the solid state of preexisting rocks by heat and pressure (e.g., gneiss, schist, hornfels, metaquartzite).

											5	0 I	L D	E 5		IPT	UN										* T E	RR	_	IN	
TATION :					XB		RAIN UK			XF	USCS		NBELL OLOR	_		URCE TYPES	6						ERT 11		14		DRAINA DEPTH				
SG8001											GM																				: 0
9G6002					_			_							_		_	_	_	_	_			_		_ :		_	_	_	: 0
365003				23			3 13		ట్	20	SM		0YR3/3		1		2	5	2	3	1	1		3		3			. 0	2	. 0
G6004				~	0		9 2		5	95 5	ML.		0YR3/3 0YR3/3		~~		-	3	3	5	1	1	~~	-	1	1		10	. 0		1 0
G8005 :				120	ő				93 75	10			5YR4/4		82		2	3	2	3		2	20 26	3	2	4 :					1 1
GS007				120	٥		15		63	35	SM		OYR4/4				3	3	2	3	•	-	46	3	-	1		13	.0	3	: 1
GS008 :					ŏ				33	15	GH-SH		V18474		12		ຸ	3	2	3	•	-	25	2	2	5		50	^		: 0
GS009				120	ŏ		5 10		85 32	13	SP-SM		5YR4/4				2	3	2	4	•	3	58	2	3	4			.0	2	: 0
GS010					ŏ		3 15		25	20	SM		OYR4/3		12		2	3	2	3	:	3	70	2	3	4				2	: 1
GS011					ŏ		5 0		75	25	SC		5YR4/6				5	3	3	ź	:	•	70	-	÷	1		33	. •	2	: 1
GS012				200	ŏ		5 20		70	10			0YR3/4		62		2	3	2	3	:	3	41	3	2	4		70	^	î	: 0
G8013				200	ŏ		20		60	20			0YR4/4				2	5	2	3	•	3	20	2	1	5				3	. 0
GS014				20	ŏ		0 20		70	30	SM		5YR5/4				2	ĭ	2	3	î	7	20	2	ì	1			. 0	i	: 0
G6015				90	ŏ		10		20	20	SM		OYR3/3				ź	3	ź	2	i	2	40	2	2	4 :		10			: 0
GS016					ŏ				53	3			OYR3/3		12		5	3	1	5	•	-	₩.	2	í	3			.0	5	-
GS017			i	110	•	٠	_	•	33	,	ar - an	10.	V 1 K3/ 3	34	12		~	•	•	~	•			~		ъ.	3.0		. •	•	1 1
GS018				85	٥		3		80	15	SM	10	0YR3/4	6.3			2		1	2	1	3	20	2	2	4	10.0	20	^		: 6
GS019				83	ŏ		3		15	85	ML		01R4/3				-		3	ź	i	1	20	2	1	1		200		6	: 8
GS020				25	ŏ		5		90	15	SH		0YR3/4		64		2	1	2	ź	i	4	35	2	2	5				2	: 0
BS021			;	23	•	•	, ,	•	~	13	311	10.	V 1 N.37 4	32	3.		- 4	•	~	~	•	•	33	~	-	٠,		200	٠.٧	2	1 1
65022			:																												: :
08023			•	75	٥		15		70	15	SM		0YR3/4	-	+2	TA 61	2		3		1	3	20	-	2						: 6
GS024				/3	ŏ		10		á	10			01R3/4			14 21	2	1	2	3	1	•	20	2	2	2				,	: 0
08025				85	ŏ		20		33	25	* SM		01R3/4			* 4	2	•	ź	3	•	1	27	2	ź	5			۰.	?	
GS024				310	ŏ		5 30		33	15	SH		01R3/4				ź	1	3	-	•	•	2/		2	3				6	: 1
BS027				20	ŏ		10		75	15	SH		01R3/4			14	2	i	2	3	:			2	2	5		90	. 0	8	: 0
G5029				20	ŏ		10		73	15	SM		0YR4/4				2	1	2	2	:	7	15 27	2	2	5				2	; 0
GS029				70	ŏ		3 3		80	15	SM		OYR3/4			*~	ź		ź		:	3	25	ź		5		_			: 0
G8030				25	ă		Ó		90	13	SP-SH		0YR3/4		31	12	2	1	1	2	1	•	23	2	2	2		35	. •	2	: 0
G8031			i	25	٠	•	•	•	70	•	3FGF	, ,,	VIRGIT	12			2		•	•		1		~	3	٠,				2	1 1
06032				45	٥		5		70	-	* SC	-	5YR4/6				-		-	_				-	3		•			2	_
98033				33	ŏ		10		65		* SK		OYR3/4					3	3	:	:	-	~	4						-	: 1
BB034				15	ŏ		5 6		95 95	5	SP~SM		01R3/3		13		3	1	i	4	3	3	25	2	2	5				:	: 1
38035				120	ŏ				95 85	10			OYR4/4		62	**	3	1	2	3	3	1	40	2	1	1 5				1	: 0
		I2	i	*50	•	•	, ,	,	-	10	ar-an	10.	V 1 R 7/ 7		34	13	3		~	~	•	-	₩	~	2	3				9	: 1
66037				30	٥				95	5	SP-SM	-	0YR3/3				3		2					2	2						: 0
G6038				75	ŏ				60 60	10			OYR5/4			٠.	2	1	2	3	1	3	24	2	1	1 1		77	^	1	: 3
G8039				100	ŏ		10		80	10			01R3/4				3	1	2	3	1	1		ź	•	3		33	.0		: 0
G6040				140	ŏ		55		35	10	GP-GM		V 1 1 7 / 4		S1	14	2	1	3	3	3	2	32	2	1			20.		1	: 0
G8041				137	ŏ		10		73	15	SH		OYR4/4				2	:	3	3	•	4	55	2	1	5 1				à	1 1
GS042			i	4/	•	٠,	- 10	•	, ,	13	381	10.	V	32	31		2	•	4	3		-	33	~	1	٠,		33	. 0	•	- •
GS043				65	٥) 10		75	15	SM	10	OYR4/4	6-			-		-	2			38	-				450	^		: 0
GS044			:	35	ŏ		, 10		/3 95	15			0YR4/6		31		4		1	4		7	30	2	1	2 :		+ 3 0	. 0	٠	: 0
G8045				35 25	ŏ		, ,		90	5			01R4/4				•		:	;		1			-					1	: 0
08045 08046		ASIS		45			9 0		97 97	3	SP-SR				21		1	1	1	3	:	1	**	2	1	_		***		-	
GS047			:	80	٥		5		92	3	SP SP		0YR5/4			~	3	•	:	÷	:	3	40	2	1					2	: 0
IGS048				45	ö		ם כ		55 55	45	SM	10.	0YR4/4	12	31	52	3	1	1	3	1	3	30	2	2	3 :		40	. 0	2	: 0
	•	~4 3	•	40	•	•	, 0	•	J	43	30						3	1	2	3	1	1		2	1	2 :				1	: 1

EXPLANATION SPHYSICAL PROPERTIES

6:GRAIN SHAPE 7:MOISTURE CONTENT 8:PLASTICITY OF FINES

: 9:CONSISTENCY :10:STRUCTURE :11:CEMENTATION-INDURATION

1121DEPTH TO CEMENTED LAYER(CH):151CALICHE DEVELOPMENT 1131MEATHERING OF CLASTS INDITE: OFOCCASIONAL(1-5X) 1144SOIL PROFILE DEVELOPMENT INDITE: SHLAB DATA



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GEOLOGIC STATION DATA MULESHOE VALLEY, NEVADA

30 JUN 81

E-TR-27-MS- <u>II</u>	
Station No.	ed Geol. Unit
Date Complete	e Geol. Unit
Observers Field Pt	noto Nos.
Air Photo No Sample ((No=0, Yes=1)
SOIL PROPERTIES	mP3 4 5 5 F
 Grain-Size Distribution: MPS (mm) - grain size of coarsest fraction; boulders and cobbles - percent of total; gravel, sand and fines - percent less than 3 inches. 	20 21 22 23 24 23 24 27
2. USCS Symbol	28 28 38 37
 Descriptive Name (one adjective only) 	
4. Munsell Color (not applicable to gravel)	32 53
 Lithology of gravel, cobbles, boulders: g type (I1, I2, N, etc.) in order of abund 	
6. Grain Shape (coarse grained soil only): 3) Subrounded, 4) Rounded, 5) Well-round	
7. Moisture Content: 1) Dry, 2) Slightly mo 5) Wet	oist, 3) Noist, 4) Very moist,
d. Plasticity of Fines: 1) None, 2) Low, 1	3) Medium, 4) High
9. Consistency: Coarse-grained: 1) Very Loose, 2) Loos 5) Very Dense Fine-grained: 6) Soft, 7) Firm, 6) S	
10. Structure: 1) Non-stratified (homogeneou 3) Stratified-other; if 3) describe	
11. Cementation-Induration: 1) None, 2) heak	, 3) Moderate, 4) Strong
12. Depth to Cemented Layer (cm)	33 34 157 ·
13. Weathering of boulders, cobbles, and grave 1) Fresh, 2) Slight, 3) Moderate, 4) Ver	
14. Degree of Soil Profile Development: 1) : 2) Poor (incipient E-horizon), 3) Well (Describe	
15. Degree of Caliche Development: 1) None, 3 4) Stage Describe	2) Stage I, 3) Stage II, III, 5) Stage IV
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	FIELD DATA SHEET PAGE 1 OF 2
	30 JUN 81 FIGURE IT-2-1

1 3.	RAIN
16.	Average Drainage Depth (ft)
17.	Average Drainage Width (ft)
18.	Slope (percent) - field and/or topo map measurement
SUF	FACE FEATURES
19.	Pit Depth (cm)
20.	Thickness of Vesicular Silt (cm)
21.	Desert Pavement Development (None, Poor, Moderate, Well)
22.	Patina Development (None, Moderate, Well)
ROC	K DESCRIPTIONS
23.	Rock Type/Formation
24.	Color, Grain size, Hardness, Texture
25.	Degree of Weathering
26.	Structure Bedding Characteristics
	Bedding Attitude
	Fracture, Joint
	Secondary Alteration/Mineralization



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FIELD DATA SHEET PAGE 2 OF 2

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FIGURE IT-2-1

3.0 GROUND-WATER DATA

Explanation: The only ground-water data available for Muleshoe Valley was a single boring recorded by the State of Nevada Engineer's Office. These data were updated where possible from measurements taken during Ertec EWI's field operations. All data are shown in Table II-3-1. The location of the borehole in which the water-level measurement was attempted is shown in Drawing II-1-1. The well number listed in the left-hand column of Table II-3-1 refers to the well location shown on Drawing II-1-1. The actual well number giving location, according to the Bureau of Land Management Land Survey System, is shown in the second column.

WELL NO.	WELL LOCATION NUMBER*	ELEVATION OF GROUND SURFACE - FEET (METERS) ABOVE M.S.L.	WELL - FEET (METERS)	WATER LEVEL			
				DEPTH BELOW GROUND SURFACE- FEET (METERS)	DATE	ELEVATION- FEET (METERS) ABOVE M.S.L.	REFERENCES*/ REMARKS
W-1	5N/64E-11cbd	5680 (1731)	290 (88)	dry	5 - 80	<5390 (1643)	1
					-		
							
							
		· 					
							<u> </u>
				<u> </u>			

- * MOUNT DIABLO BASELINE AND MERIDIAN
- **REFERENCES:
 - 1. ERTEC WESTERN MEASUREMENT



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GROUND - WATER DATA
MULESHOE VALLEY, NEVADA

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TABLE II-3-1

4.0 SEISMIC REFRACTION DATA

Explanation: Each figure shows seismic wave travel times plotted versus surface distance between the energy source (shot) and the detector (geophone) for a single seismic line. Distances are measured along the line from geophone number 1 which is designated as zero distance. Distances to the right (on the paper) of geophone 1 are positive. The direction arrow gives the approximate direction of the geophone array from geophone 1 to geophone 24.

Travel Time Versus Distance Graph (Upper Half of Figure)

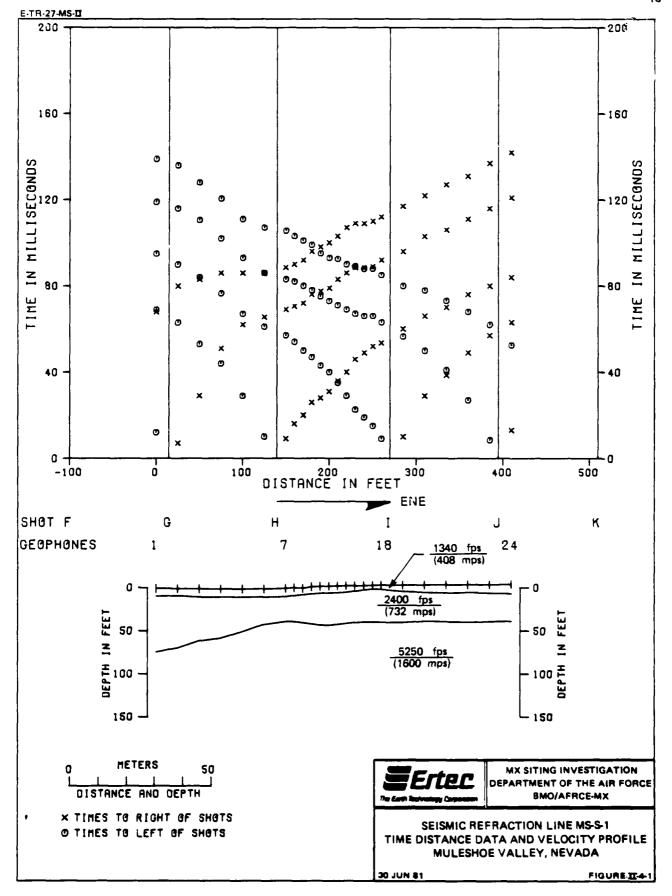
On this graph, the abscissa represents distance; the ordinate, time. The six vertical lines represent the locations of shots (designated as F, G, H, I, J, and K). The symbol "X" denotes travel times at geophones that were located to the right of a shot. The symbol, Θ , denotes travel times that were located to the left of shots.

Velocity Cross Section (Lower Half of Figure)

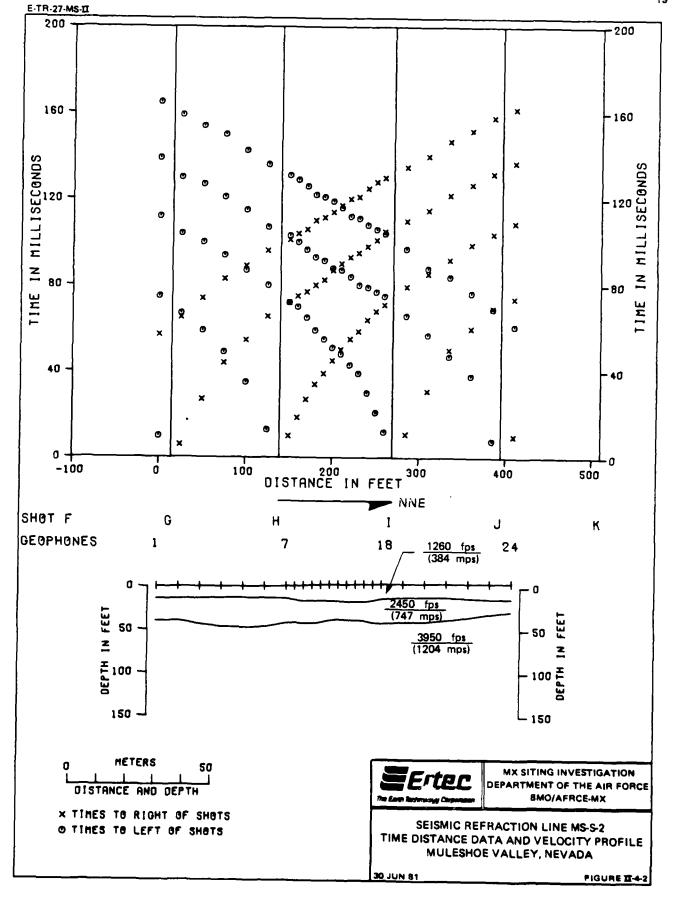
This is an interpreted velocity cross section beneath the seismic line. The top line represents the ground-surface profile. The short vertical lines crossing the top line mark the geophone positions. The depth scale is plotted relative to a point on the line which was arbitrarily chosen as "zero elevation" at the time the line was surveyed. The additional lines across the cross section represent the interpreted boundaries between layers of material with different compressional wave

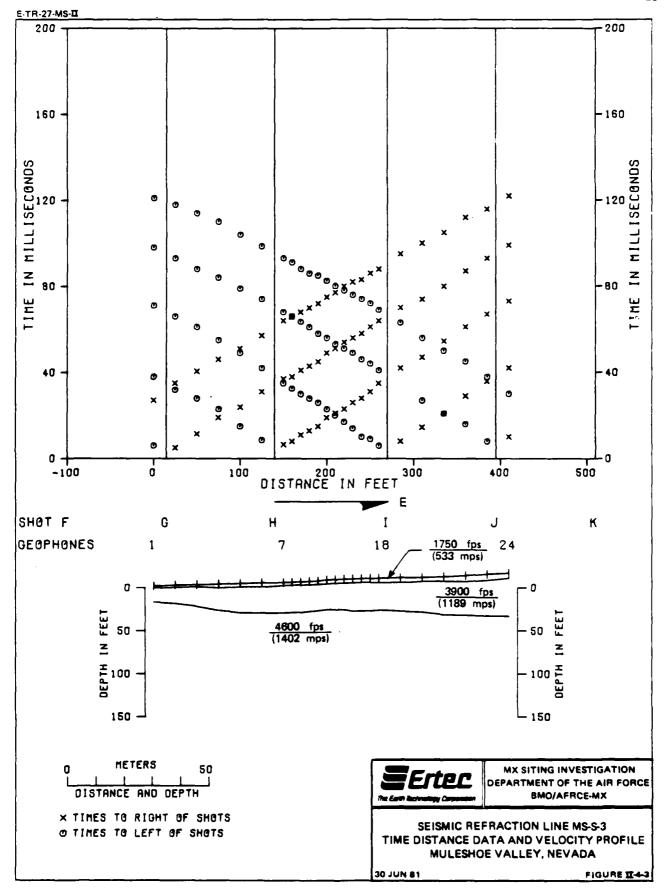
velocities. These boundaries are commonly called "refractors."

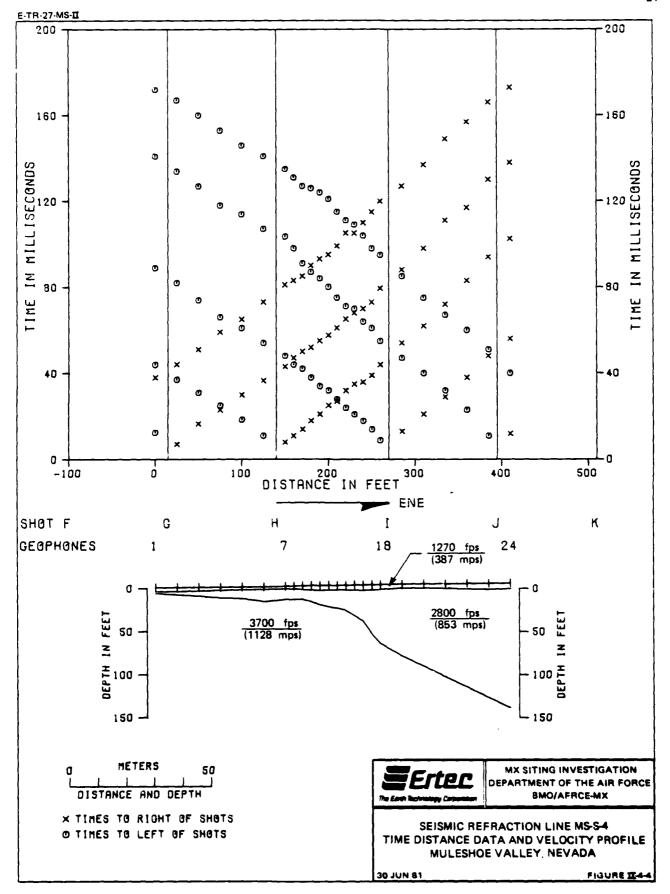
The velocity interpreted to be represent tive of each layer is shown.

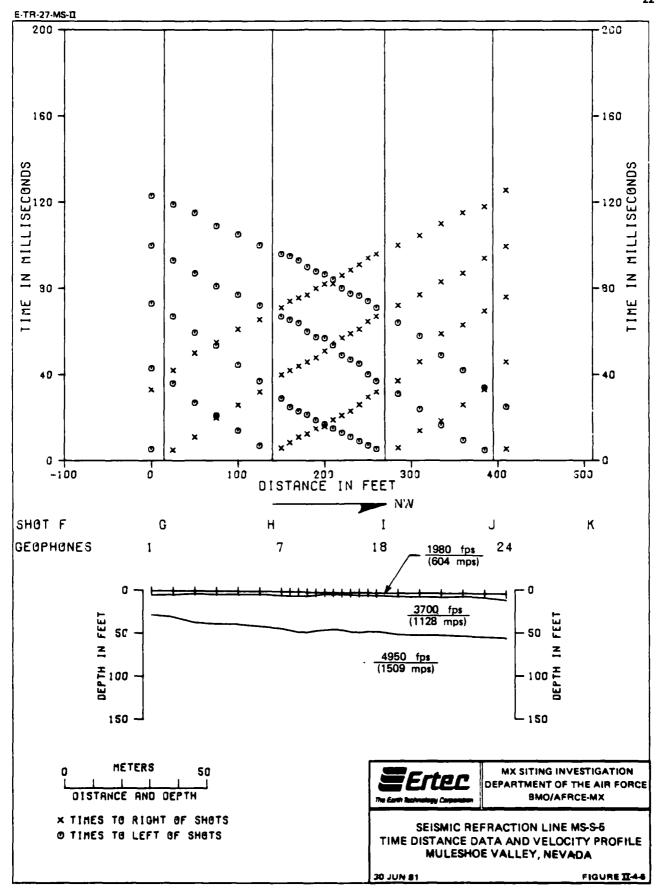


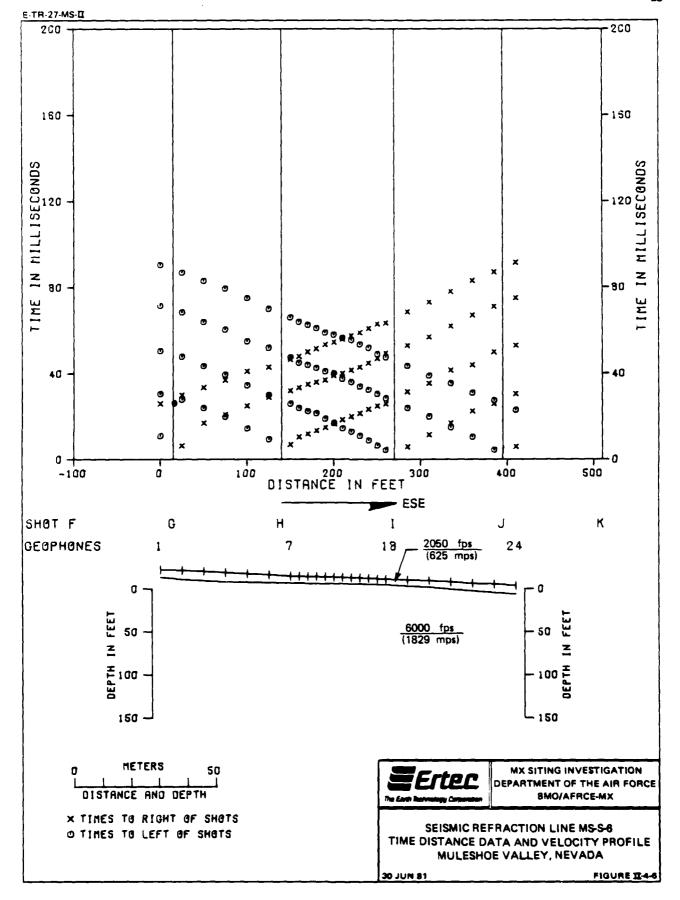
and measurement and appropriate and

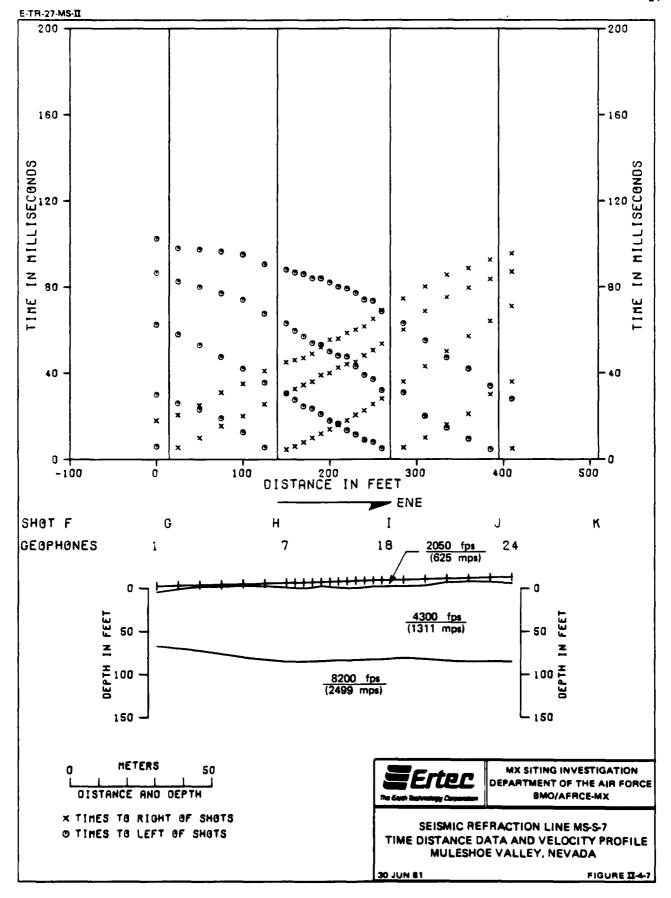


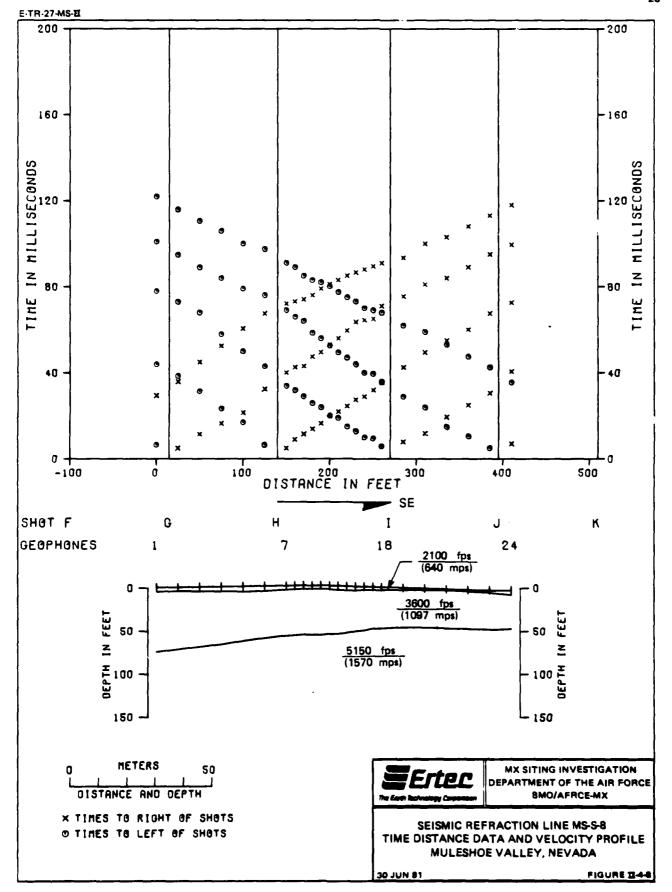


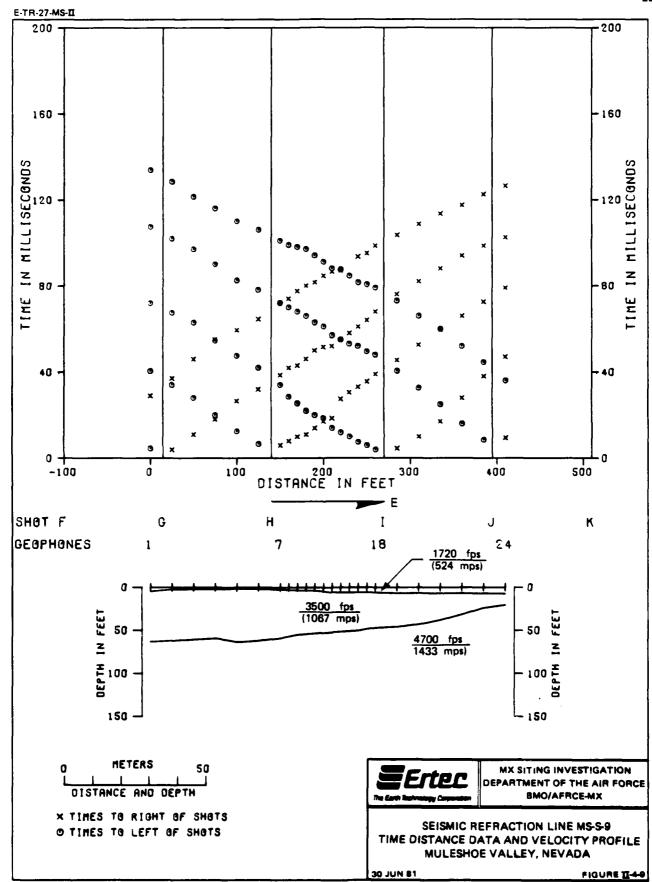


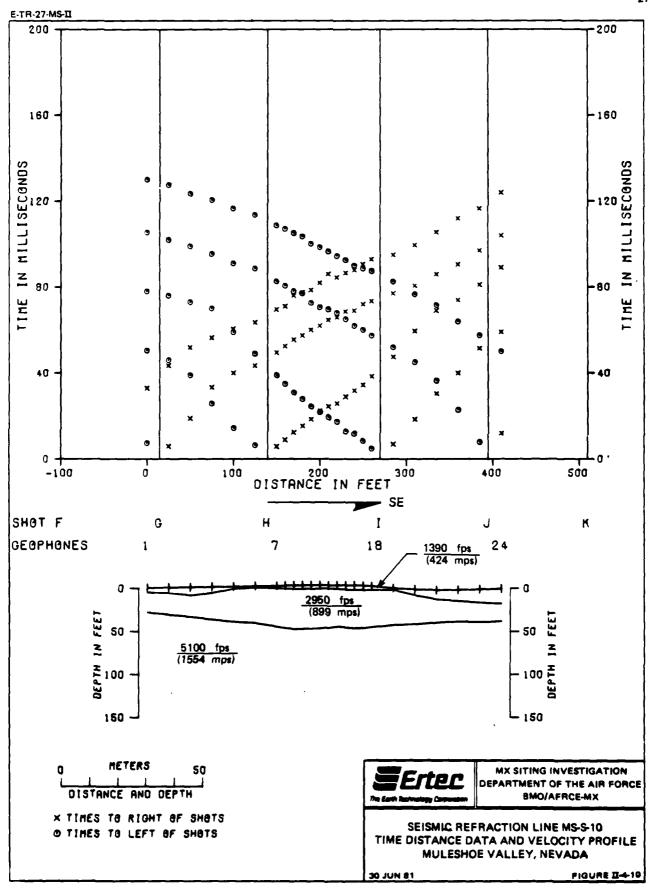












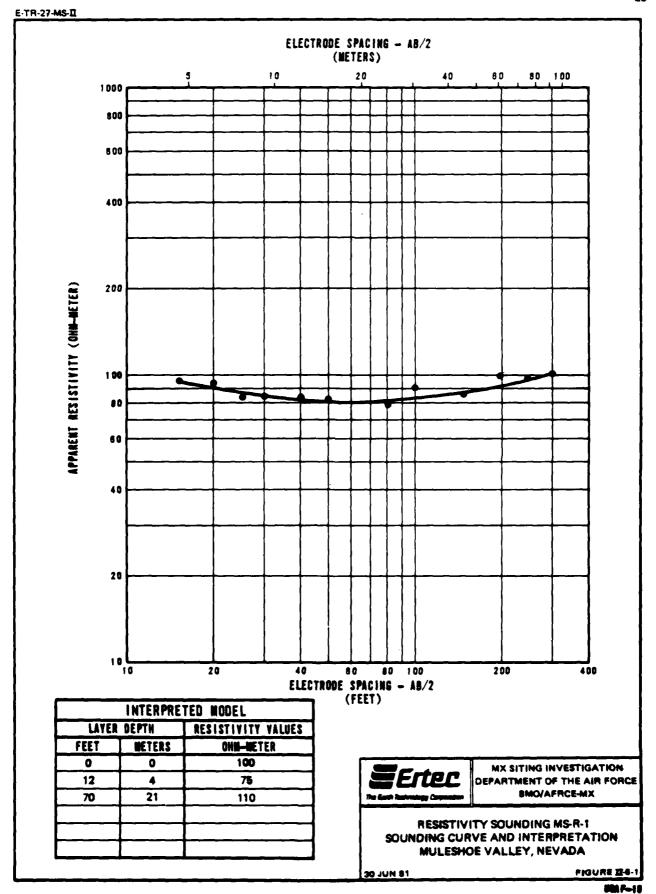
5.0 ELECTRICAL RESISTIVITY DATA

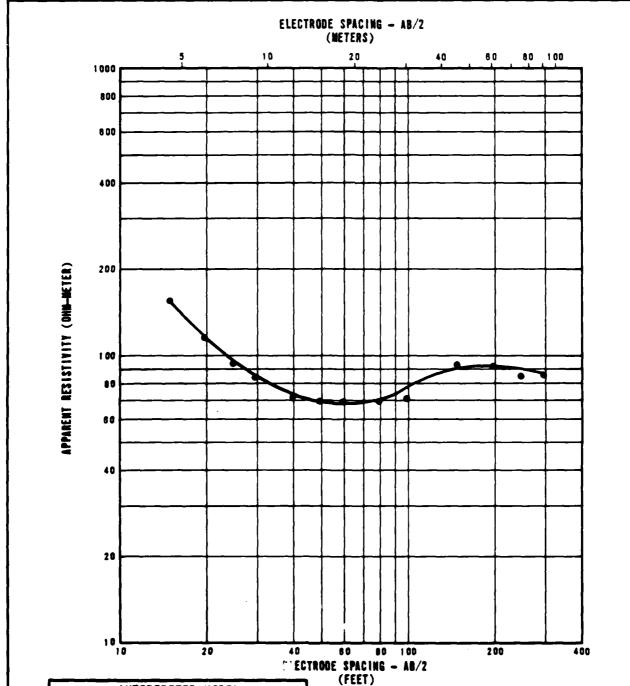
Explanation: Each figure in this section presents the data obtained from a resistivity sounding and a tabulated model of resistivity layers that would produce a curve similar to the observed curve.

The upper portion of the figures is a graph in which measured apparent resistivity values in ohm-meters are plotted versus one-half the distance between the current electrodes.

The interpreted model tabulated at the bottom of the page shows a combination of true resistivity layers and thicknesses obtained by matching theoretical curves to the field curve.

Note: There was no resistivity sounding at location MS~SR-2 because of electrical interference from a grounded fence.





	INTERPRE	TED MODEL
LAYER	DEPTH	RESISTIVITY VALUES
FEET	METERS	OHW-WETER
0	0	250
7	2	66
55	17	110
176	54	60
	 	<u> </u>
	1	i

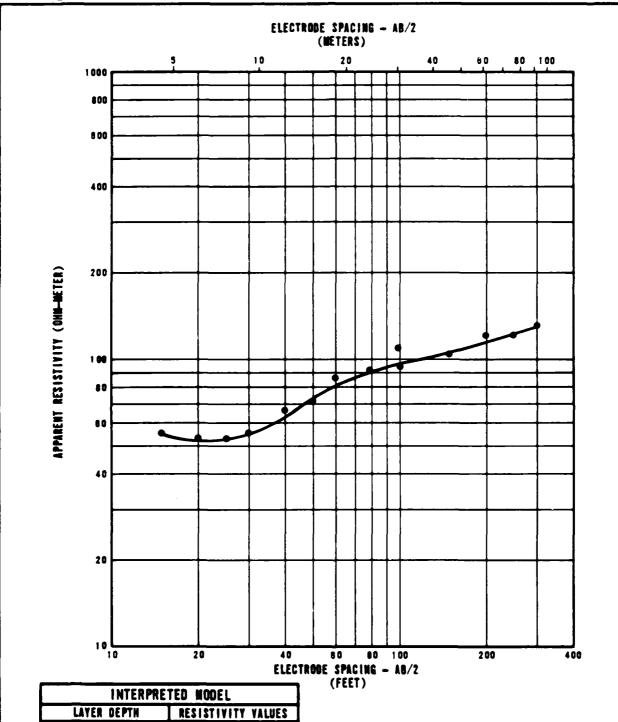
EErtec

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RESISTIVITY SOUNDING MS-R-3 SOUNDING CURVE AND INTERPRETATION MULESHOE VALLEY, NEVADA

30 JUN 81

FIGURE 2-8-2



	INTERPRETED MODEL						
LAYE	R DEPTH	RESISTIVITY VALUES					
FEET	METERS	OHM-METER					
0	0	50					
25	8	280					
32	10	110					
163	50	250					
	1						

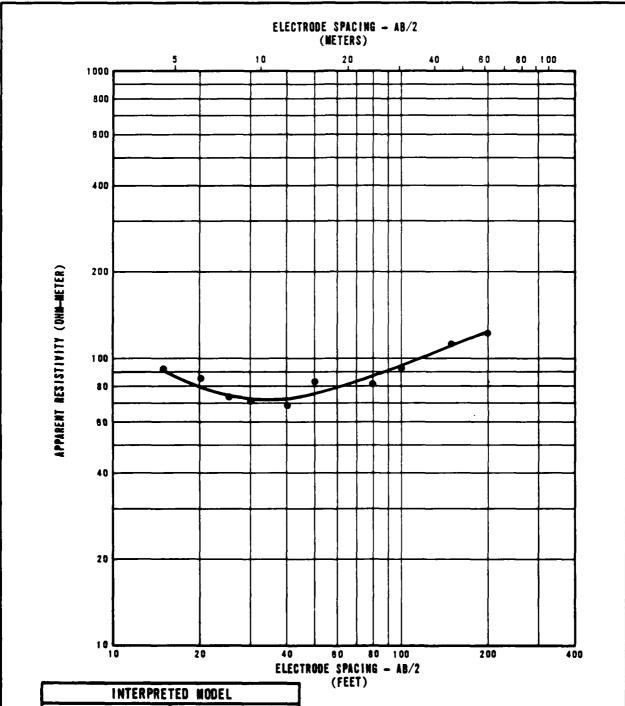


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RESISTIVITY SOUNDING MS-R4
SOUNDING CURVE AND INTERPRETATION
MULESHOE VALLEY, NEVADA

30 JUN 81

FIGURE II-6-3



	INTERPRETED MODEL						
LAYE	DEPTH	RESISTIVITY VALUES					
FEET	METERS	OHM-METER					
0	•	120					
5	2	80					
50	15	150					

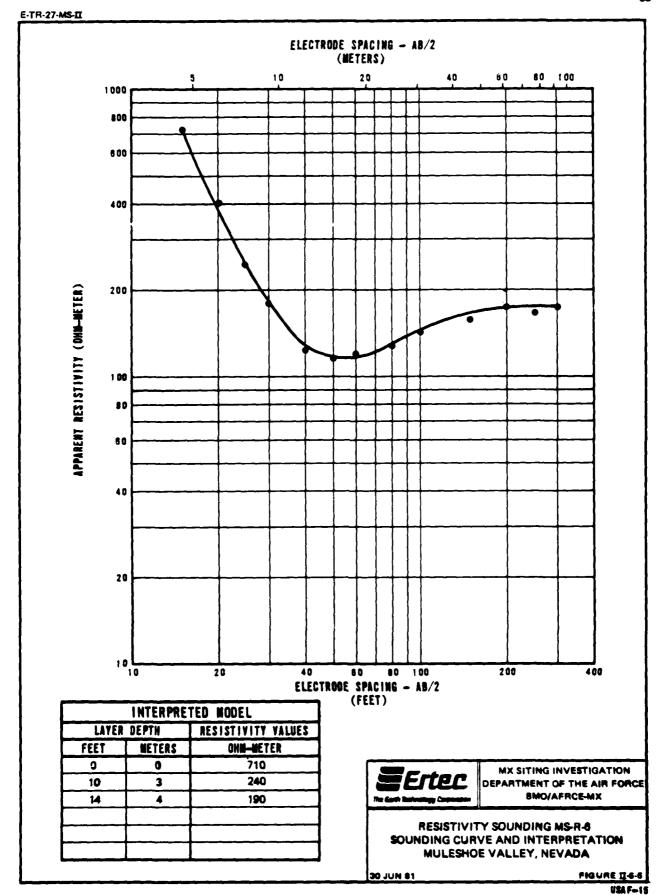


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RESISTIVITY SOUNDING MS-R-5
SOUNDING CURVE AND INTERPRETATION
MULESHOE VALLEY, NEVADA

30 JUN 81

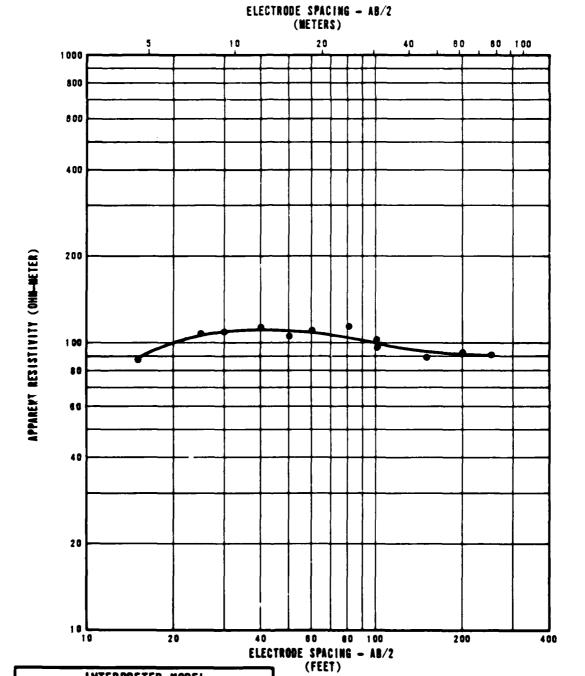
FIGURE 12-6-4



RESISTIVITY SOUNDING MS-R-7 SOUNDING CURVE AND INTERPRETATION **MULESHOE VALLEY, NEVADA**

30 JUN 81

FIGURE IL-6-6



	INTERPRETED MODEL					
LAYER	R DEPTH	RESISTIVITY VALUES				
FEET	METERS	ONIN-METER				
0	0	66				
5	2	130				
29	9	80				
90	27	110				
	T T					

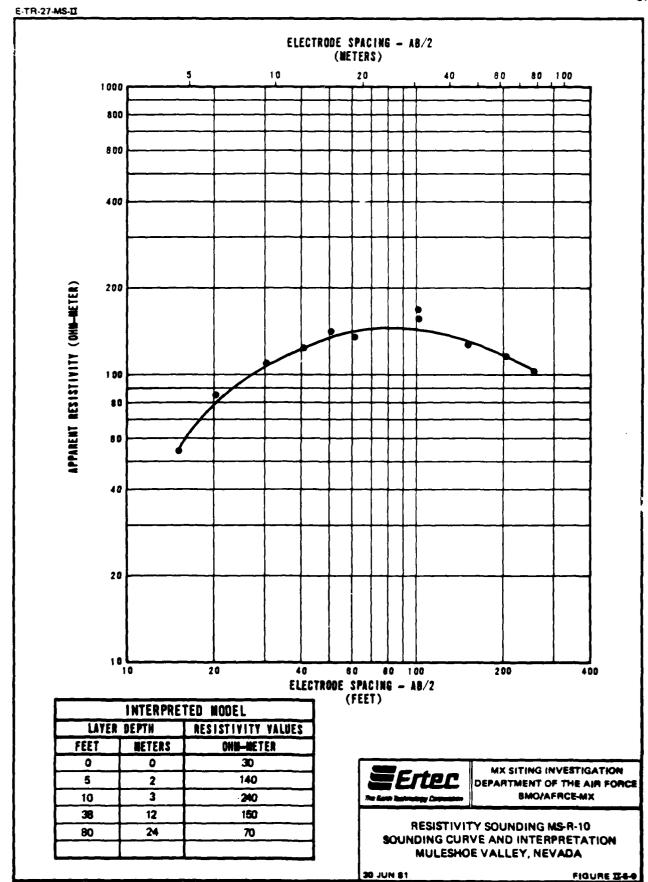


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RESISTIVITY SOUNDING MS-R-8
SOUNDING CURVE AND INTERPRETATION
MULESHOE VALLEY, NEVAD:

30 JUN 81

FIGURE II-4-7



6.0 BORING LOGS

Explanation: All data from borings, trenches and test pits are presented on standard Ertec Western logs in Sections 6.0 and 7.0. Explanations of the column headings on the logs are as follows:

A. Designations - Borings and trenches are identified as follows:

MS-B-1

MS - abbreviation for the valley (e.g., MS Muleshoe)

B - abbreviation for activity (e.g., B-boring, T-trench, P-test pit)

l - number of activity

- B. Sample Type Different sampling techniques were used and the symbols are explained at the bottom of the boring logs. For details of sampling techniques, see Section A5.0 of Appendix in Volume I (E-TR-27-MS-I). Horizontal lines, to scale, indicate the depth where sampling was attempted.
- C. Percent Recovery The numbers shown represent the ratio (in percent) of the soil sample recovered in the sampler to the full penetration of the sampler.
- D. N Value Corresponds to standard penetration resistance, which is number of blows required to drive a standard split-spoon sampler for the second and third of three 6-inch (15-cm) increments with a 140-pound (63.5 kg) hammer falling 30 inches (76 cm) (ASTM D 1586-67).
- E. Depth Corresponds to depth below ground surface in meters and feet.

- F. Lithology Graphic representation of the soil and rock types.
- G. USCS Unified Soil Classification System symbols (see Table II-6-1 for complete details).
- H. Soil Description Except in cases where samples were classified based on laboratory test data, the descriptions are based on visual classification. The procedures outlined in ASTM D 2487-69, Classification of Soils for Engineering Purposes, and D 2488-69, Description of Soils (Visual-Manual Procedure), were followed. A solid line across the column indicates change in strata at the depth shown.

Definitions of some of the terms and criteria to describe soils and conditions encountered during the exploration follow.

Gradation: A coarse-grained soil is well graded if it has a wide range in grain size and substantial amounts of most intermediate particle sizes.

Poorly graded indicates that the soil consists predominantly of one size (uniformly graded) or has a wide range of sizes with some intermediate sizes obviously missing (gap-graded).

Moisture: Dry - no feel of moisture - dry like powder

Slightly Moist - much less than optimum mois-

ture
Moist - near optimum moistu:

 near optimum moisture for soil - provides apparent

cohesion

Very Moist - much greater than optimum moisture

- at or near saturation

Consistency: Consistency descriptions of coarse-grained soils (GW, GP, GM, GC, SW, SP, SM, SC) follow.

Wet

(Excluding per	perticles larger than 3 in estimated west		roccourts sad being fractions on hts?	uo	Symbols	Typical Names	Describing Soils			Criteria Criteria	- 1
321 0 0 41	ETRYCLE Of DO (EDG)	Wide range in smounts o	bage in grain size and substantal	d substantial	à	Well graded gravels, gravel- sand mixlures, little or no fines	Give typical name, indicate ap- proximate percentages of sand		jo sen swoji on ut	$C_U = \frac{D_{10}}{D_{10}}$ Greater than 4 $C_0 = \frac{(D_{10})^3}{D_{10} \times D_{10}}$ Beingen J and	7 3
i jo lier Istat Serve Served	Clean	Predominanti with tome	inantly one size or a range of sizes some intermediate sizes missing	ange of sizes	45	Poorly graded gravels, gravel- sand mixiures, little or no fines	and gravel, maximum size, angularity, furface condition, and hardness of the coarse		di talla o) as bo ammu	Not meeting all gradation requirements for GW	3
(a) (a) (a) (a) (a) (a) (a) (a) (a) (a)	JO 10 SIQUES SI MILE SI MILE	Nonpla	sic Bots (for idealification pro- us set ML below)	Kation pro-	N C	Silty gravels, poorly graded gravel-sand-silt mixtures	and other periodes descriptive information, and symbols in parentheses	uc	tion 28. W 28. W 48. SP 10011300 Sm	Atterberg limits below "A" line, or PI less than a	Above "A" this with P! between 4 and 7 are
ya badan ya badan solM solM	(avata) ang arqqa) arqqa auoma	Plante 6	nes (for identification procedures, L'below)	procedures,	ÿ	Clayey gravels, puorly graded gravel-sand-clay muxtures	3 2 4	HI BODILU:		Atterberg Jimits above "A" line, with PI greater than 7	borderline cases requiring use of dust symbols
COSTRE COSTRE	on sends on so se or no	Wide range in amounts of	ide range is grain tizes and substantial amounts of all intermediate particle times	substantial	à S	Well graded sands, gravelly sands, little or no fines	moisture conditions and dhinage characteristics Example Sily sand, gravelly; about 20%		d Bornsteiner Bornsteiner Com Schiege of f	$C_U = \frac{D_{10}}{D_{10}} = \frac{Greater than}{(D_{20})^3}$ $C_C = \frac{(D_{20})^3}{D_{10} \times D_{30}} = \text{Betwee}$	r than 6 Between 1 and
starse starse starse lo liant soliams seve se	Chu	Predominanti with some	unantly one size or a range of sizes pome intermediate sizes missing	ange of suce	3	Poorly graded sands, gravelly sands, little or no fines	hero, anguar gravel particles i-in maximum size, rounded and aubangular sand grains	oun 43/	", " l y u u y co (3211 co (3211 co (beta	Not meeting all gradation requirements for SW	requires
re then is Clion is No.4 s	with sates in of tallocates	Nompta	onplastic fines (for identification pro- cedures, see ML below)	Scation pro-	NS.	Sily sands, poorly graded sand- silt mixtures	plastic fines with low dry strength, well compacted and moust in place, allowed sand;	ns as en	arve Sending Server More t of 4% to	Atterberg limits below "A" line or Priess than	Above "A" line with PI between 4 and 7 are
oM anì	id iqqa) ioms	Plantic O	ines (for identification procedures, L'below)	procedures.	, ,	Clayey sands, pourly graded sand-clay mistures	(WC)	ionogal Iod	Del	Atterberg limits below "A" line with P!	borderline cases requiring use of dual symbols
Identification	Procedures	on Fraction Smi	Fraction Smaller than No. 40 Sieve Size	O Sieve Size	1			343			
SI SEIS DA		Dry Strength (crushing character- nites)	Dilatancy (reaction to shaking)	Toughness (consistency near plastic limit)				Butking	60 Comparing		
c size	06 nadi	None to	Quelt to	None	¥	Inorganic silts and very fine sands, tick flows, silty or clarcy fine sands with slight plassicity	Give typical name, indicate degree and character of planicity, amount and maximum size of		انالین ع	Suginess and day streety incresse	
estic epit	1634	Medium to	None to	Medium	3	inorganic clays of low to medium plasticity, gravelly clays, sandy clays, silty clays, lean clays	condition, odous if any, local or geologic name, and other pertinent descriptive information, and symbol in perentheses	asis mist Charles Passing	S S		3.
oN a		Slight to medium	Nogs .	Stugat	70	Organic salts and organic salt-	For undisturbed soils add infor-		10		I.
clays hmit than the		Slight to medium	Show to Rune	Slight	NN	Inorganic silts, misscents or distornaceurs fine sandy or s.ity soils, elastic silts	Faiton on structure, stratting, two, consistency in undisturbed and remounded states, monsture and distincts conditions		1 0	20 30 40 50 60 70	a
put i	06	Heh to	a do Z	=	3	Inorganic clays of high plas-	Example	_		Ciquid fimit	
M		Medicin to	None to	Slight to	KO	Organic clays of medium to high	Clayer sill, brown; slightly plastic, small percentage of		for laboral	Plasticity chait for laboratory classification of time example soils	01310
Highly Organic S	Souts	Readily iden	identified by colour, odour,	our, odour,		Peat and other highly organic	not take. from and dry in				

These procedures are to be performed on the minus No. 40 serve use particles, approximately Yis, in Por field classification for channels and to channels are all cube controlled to the control of particles tracer in the color hand server in the server in the particles to the pa

Toughest (Consistency near plants limit) (9. 40 three tag, a specimen of After tennous partials larger than the 10 solubles tag, a specimen of After tennous partials larger than the 10 solubles tag, a specimen of the 10 solubles to 10 sol simply remove by hand the coarse particles that interfere with the tests

MX SITING INVESTIGATION DEPARTMENT OF THE AIR FORCE **BMO/AFRCE-MX**

UNIFIED SOIL CLASSIFICATION SYSTEM

TABLE IL-6-1

30 JUN 81

	N Value
Consistency	(ASTM D 1586-67)
Very Loose	0 - 4
Loose	4 - 10
Medium Dense	10 - 30
Dense	30 - 50
Very Dense	>50

Consistency descriptions of fine-grained soils (ML, CL, MH, CH) are as follows:

		Shear St	trength				
	Consistency	(ksf) ()	(n/m^2)	Field Guide			
	Very Soft	0.25	12	Sample with height equal to twice the diameter, sags under own weight			
	Soft	0.25- 0.50	12 - 24	Can be squeezed between thumb and forefinger			
	Firm	0.50- 1.00	24- 48	Can be molded easily with fingers			
	Stiff	1.00-2.00	48- 96	Can be imprinted with slight pres- sure from fingers			
	Very Stiff	2.00- 4.00	96- 192	Can be imprinted with considerable pressure from fingers			
	Hard	over 4.00	over 192	Cannot be im- printed by fingers			
Grain Shape:	Angular -	relative		sharp edges and e sides with aces.			
	Subangular -			imilar to angular at rounded			
	Subrounded -	sides bu	particles exhibit nearly plane sides but have well-rounded corners and edges.				

Rounded - particles have smoothly curved sides and no edges. Calcareous : Containing calcium carbonate; presence of calcium carbonate is commonly identified on the basis of reaction with dilute hydrochloric acid. Caliche : Soils cemented by calcium carbonate and/or other soluble minerals by upward-moving solutions. Degree of Cementation: (Stages of development of caliche profile) Stage Gravelly Soils Nongravelly Soils Thin, discontinu-Few filaments or ous pebble coatings faint coatings ΙI Continuous pebble Fee to abundant coatings, some nodules, flakes, interpebble fillfilaments ings III Many interpebble Many nodules and fillings internodular fillings IV Laminar horizon Increasing carbonoverlying plugged ate impregnation horizon Secondary Material Example - Sand with trace to some silt Trace - 5-12% (by dry weight) Little - 13-20% (by dry weight) Some - >20% (by dry weight) Plasticity: Plasticity index is the range of water content, expressed as a percentage of the weight of the oven-dried soil, through which the soil is plastic. It is defined as the liquid limit minus the plastic limit. Descriptive ranges used on the logs include: Nonplastic (PI, 0-4) Slightly Plastic (PI, 4-15)

Highly Plastic (PI,

Medium Plastic (PI, 15 - 30)

Cobbles and Boulders :

: A cobble is a rock fragment, usually rounded by weathering or abrasion, with an average diameter ranging between 3 and 12 inches (8 and 30 cm).

A boulder is a rock fragment, usually rounded by weathering or abrasion, with an average diameter of 12 inches (30 cm) or more.

- I. Remarks This column was provided on boring and trench logs for comments regarding drilling difficulty, number and size of cobbles or boulders encountered, loss of drilling fluid in the boring, trench wall stability, and other conditions encountered during drilling and excavations.
- J. Dry Density and Moisture Content The boring logs include a graphical display of laboratory test results for dry density (ASTM D 2937-71) in pounds per cubic foot and kilograms per cubic meter and moisture content (ASTM D 2216-71) in percent from representative samples taken during drilling. The symbols are explained at the bottom of the boring logs.
- K. Sieve Analysis The numbers represent the percentage by dry weight (ASTM D 422-63) of each of the following soil components:
 - GR Gravel, rock particles that will pass a 3-inch (76-mm) sieve and are retained on No. 4 (4.75 mm) sieve.
 - SA Sand, soil particles passing No. 4 sieve and retained on No. 200 (0.075 mm) sieve.
 - FI Fines, silt or clay soil particles passing No. 200 sieve.
- L. Atterberg Limits (LL and PI) -
 - LL Liquid Limit, the water content corresponding to the arbitrary limit between the liquid and plastic states of consistency of a soil (ASTM D 423-66).

- PL Plastic Limit, the water content corresponding to an arbitrary limit between the plastic and the semisolid state of consistency of a soil (ASTM D 424-59).
- PI Plasticity Index, numerical difference between the liquid limit (LL) and the plastic limit (PL) indicating the range of moisture content within which a soilwater mixture is plastic.
- NP Nonplastic.

M. Miscellaneous Information -

Elevations - indicated elevations on the logs are estimated from topographic maps of the study area, within an accuracy of half the contour interval.

Surficial

Geologic Unit - indicates the surficial geologic unit in which the activity is located.

Date Drilled - indicates the period from beginning to completion of the activity.

Drilling

Method - signifies the type of drilling procedure used such as rotary wash.

Hole Diameter - nominal size of boring drilled.

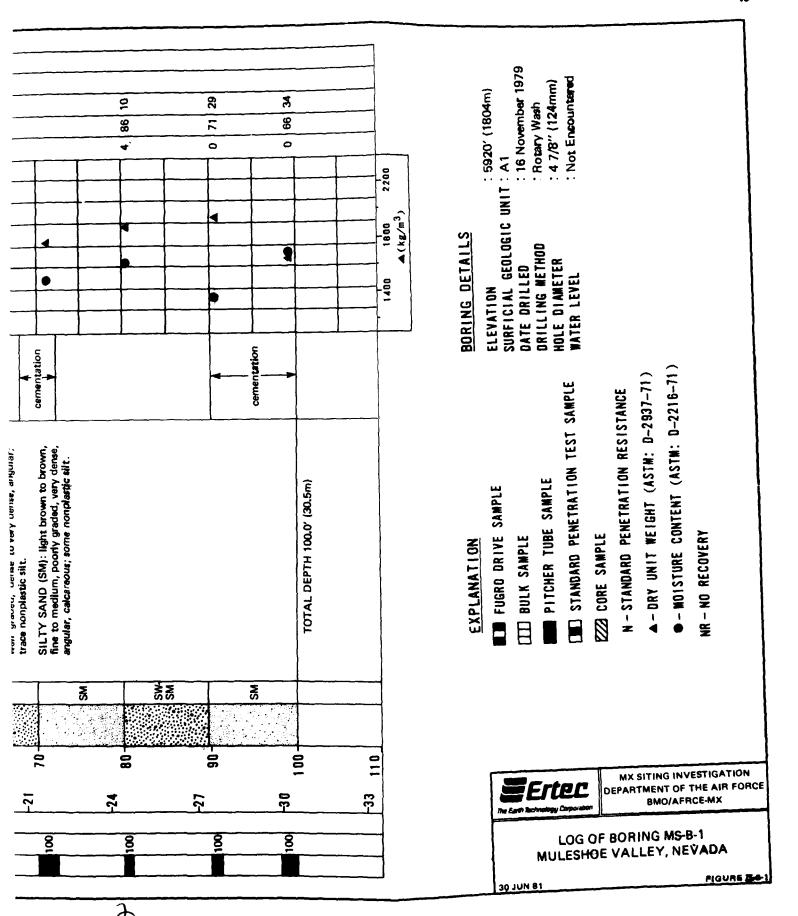
Water Level - indicates depth from ground surface to water table where encountered.

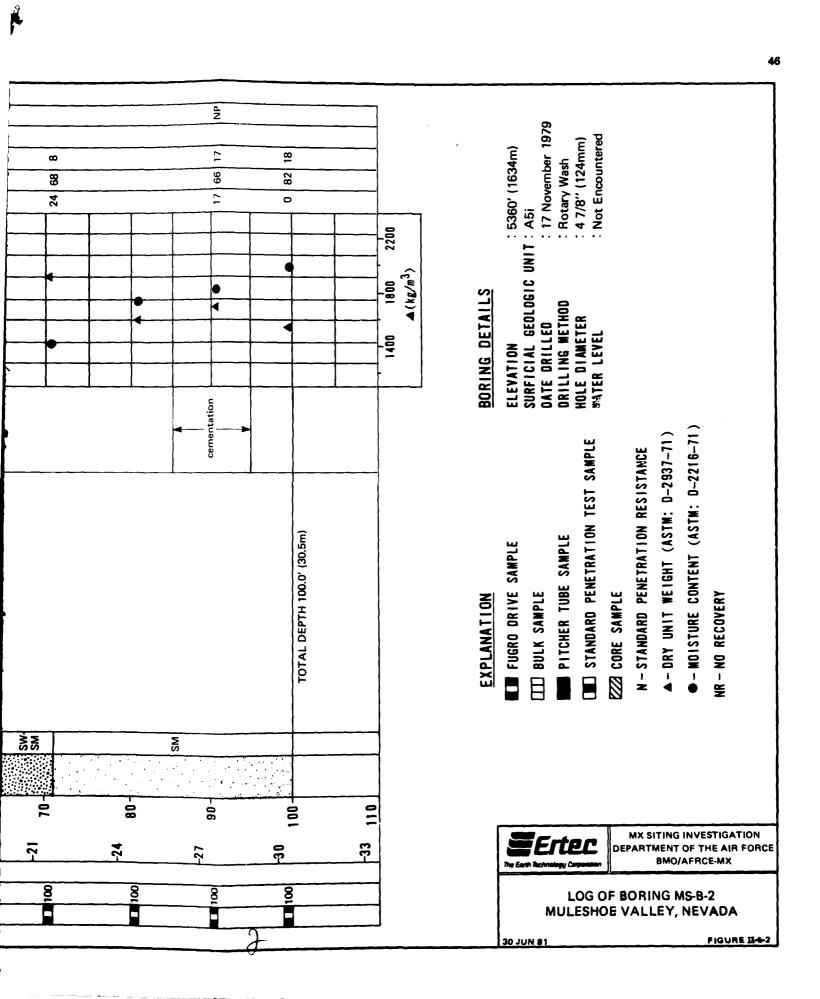
Trench Length - length at ground surface of final trench excavation.

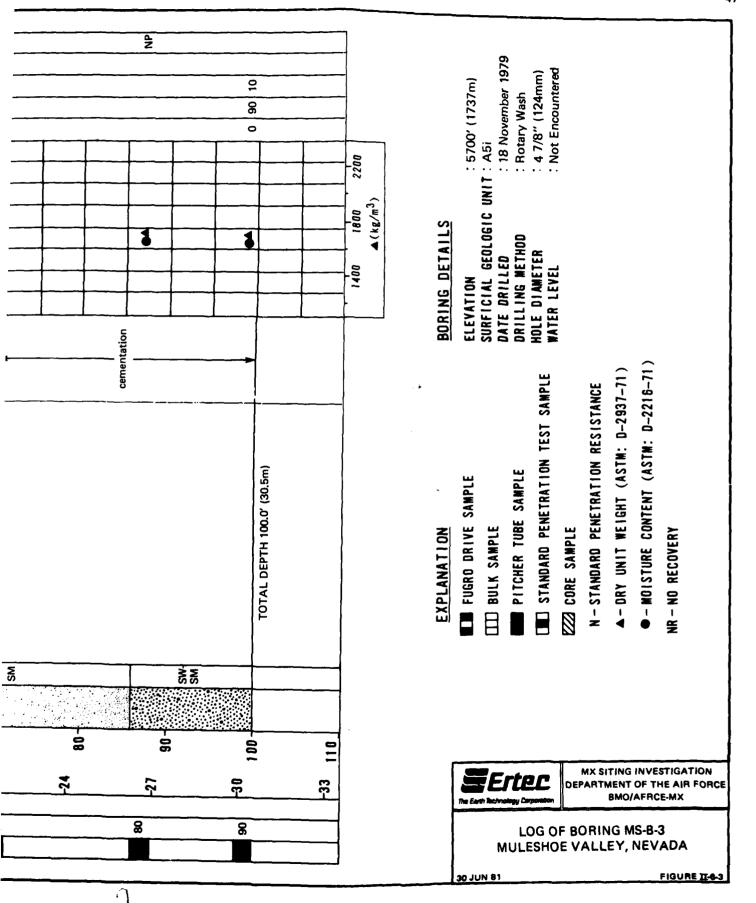
Trench

Orientation - bearing of longitudinal trench centerline.









7.0 TRENCH AND TEST PIT LOGS

See Section 6.0, "Boring Logs," for explanation.

BULK SAMPLE	METERS A	FEET	TITHOLOGY	uscs	CONSISTENCY	SOIL DESCRIPTION	REMARK	S AM	S I E V	\$15		
3		3			8			SR	SA	FI	ιL	P
	9	2-				SANDY CLAY - SANDY SILT, dark brown, slightly moist, slightly plastic, calcareous; some fine to medium subangular sand; occasional cobbles to 10" size (8.0" - 14.0").		2	26	72	25	4
	- 2	8 -		CL- ML	stiff		vertical w stable	adis				
	- 3	10-				SILTY SAND, dark brown, fine to coerse, poorly graded, slightly maint,						
	-4	14-		SM	medium dense	subengular to subrounded, calcareous; some nonplastic to slightly plastic silt. TOTAL DEPTH 14.0' (4.3m)						
						TOTAL DEPTH 14.0 (4.3m)						
	- 5	18-										
		18-										
	- 8	20-										
. 1	ľ		}	1	1		1	- 1	1	1	1 '	i

SURFACE ELEVATION : 6230' (1880m)
BATE EXCAVATED : 20 October 1979

SURFICIAL GEOLOGIC UNIT: ASI

TRENCH LENGTH : 16.0' (4.9m)
TRENCH ORIENTATION : E-W



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LOĞ OF TRENCH MS-T-1 MULESHOE VALLEY, NEVADA

30 JUN 81

FIGURE 15-7-1

BULK SAMPLE	EPTH	LITHOLOGY	uscs	CONSISTENCY	SOIL DESCRIPTION	REMARKS	AN	I EV	318	
0	2 -	n	sc	medium	CLAYEY SAND, dark brown, fine to coarse, poorly graded, slightly moist, subangular, calcareous; some slightly plastic day.			5A 600		
-2	8 -				SILTY SAND, brown, fine to coarse, poorty graded, slightly moist, subangular, calcersous; some nonplastic silt; occasional cobbles to 8" size.	vertical walls stable	1	68	31	NI
-3	10-		SM	dense						
-4	14-				TOTAL DEPTH 14.0' (4.3m)		-			
- 5	16-									
- 6	20-									

SURFACE ELEVATION : 5980' (1828m)
DATE EXCAVATED : 21 October 1979

SURFICIAL GEOLOGIC UNIT: A50 TRENCH LENGTH : 18,0° (4,9m) TRENCH ORIENTATION : E-W



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LOG OF TRENCH MS-T-2 MULESHOE VALLEY, NEVADA

30 JUN 81

FIGURE II-7-2

- W	LITHOLOGY	NSCS	CONSISTENCY	SOIL DESCRIPTION	REMARKS			SIS	L	
2 - 4 -	17	CL	sulff	SILTY CLAY, dark brown, slightly moist, slightly pleatie, calcareous; trece fine sand.		GR O			31	
8-		MAL.	Stille	SANDY SILT, brown, slightly moist, nonpleate, calcareous; some fine sub-angular to subrounded sand.	vertical wells stable	0	41	50		NP
12-		SW- SM	medium dense	GRAVELLY SAND, dark brown, fine to coarse, well graded, slightly moist, angular to subangular, catcareous; little fine subangular gravel; trace nonplastic silt. TOTAL DEPTH 14.0' (4.3m)		17	73	10		
18-										
	14-116-116-1	10-11-11-11-11-11-11-11-11-11-11-11-11-1	10 - MAL 110 - SW-SM	8 - 10 - 12 - 18 - 18 - 18 - 18 - 18 - 18 - 18	SANDY SILT, brown, slightly moist, nonpleatie, calcareous; trace fine sand. SANDY SILT, brown, slightly moist, nonpleatie, calcareous; some fine subangular to subrounded sand. SM medium dense GRAVELLY SAND, dark brown, fine to coarse, well graded, slightly moist, angular to subangular gravel; trace nonpleatic sit. TOTAL DEPTH 14.0' (4.3m)	CL stiff SANDY SILT, brown, slightly moles, nonpleatic, calcareous; some fine sub-angular to subrounded sand. SANDY SILT, brown, slightly moles, nonpleatic, calcareous; some fine sub-angular to subrounded sand. SM GRAVELLY SAND, dark brown, fine to coarse, well graded, slightly moles, angular to subangular, calcareous; little fine subangular grave; trace nonpleatic sitt. TOTAL DEPTH 14.0' (4.3m)	moist, slightly plastile, calcaraous; trace fine sand. CL stiff SANDY SILT, brown, slightly moist, nonplastic, calcaraous; some fine sub-angular to subrounded sand. SANDY SILT, brown, slightly moist, nonplastic, calcaraous; some fine sub-angular to subrounded sand. GRAVELLY SAND, dark brown, fine to coarse, well graded, slightly moist, angular or subangular, calcaraous; little fine subangular gravel; trace nonplastic slit. TOTAL DEPTH 14.0' (4.3m)	TOTAL DEPTH 14.0' (4.3m) CL stiff moist, sightly pleatie, calcareous; trace fine sand. SANDY SILT, brown, slightly moist, nonpleatie, calcareous; some fine subsequiar to subrounded sand. SW medium clease GRAVELLY SAND, dark brown, fine to corre, well graded, slightly moist, angular to subenquiar, calcareous; little fine subsequiar, calcareous; lit	TOTAL DEFTH 14.0' (4.3m) Nerrices weeks Nerrices weeks Nerrices weeks Nerrices weeks SANDY SILT. brown, slightly moles, nonplease, calcareous; some fine sub-angular to subrounded sand. Nerrices weeks SANDY SILT. brown, slightly moles, stable SANDY SILT. brown, slightly moles, stable SANDY SILT. brown, slightly moles, stable SANDY SILT. brown, slightly moles, sealer sub-angular to subrounded sand. O 41 56 10 17 73 10	CL staff SANDY SILT, brown, slightly moles, nonpleate, calcareous; trace SANDY SILT, brown, slightly moles, nonpleate, calcareous; some fine sub-angular to subrounded sand. SANDY SILT, brown, slightly moles, stable SANDY SILT, brown, sl

SURFACE ELEVATION : 5020' (1804m)
DATE EXCAVATED : 21 Occober 1979

SURFICIAL GEOLOGIC UNIT: A1

TRENCH LENGTH : 16.0' (4.9m)
TRENCH GRIENTATION : N-S



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LOG OF TRENCH MS-T-3
MULESHOE VALLEY, NEVADA

30 JUN 81

FIGURE 13-7-3

E-TR-27-MS-II DEPTH CONSISTENCY SIEVE ME TE AS SOIL DESCRIPTION REMARKS ANA LYSIS GR SA FI LL PI GRAVELLY SAND, light brown to white, fine to coarse, poorly graded, dry, angular, calcareous; some fine to coarse gravel; little nonplastic silt; stage III - IV callehe (0.5' - 4.5'). 2 vertical walls very stable TOTAL DEPTH 4.5' (1.4m) comentation at 4.5' exceeded capacity of Case 580C backhoe 6 - 2 8 - 3 10-12 14-18 - 5 18

TRENCH DETAILS

20-

SURFACE ELEVATION : 6100' (1860m)
DATE EXCAVATED : 30 October 1979

SURFICIAL REOLOGIC UNIT: A50
TRENCH LENGTH : 8.0' (2.4m)
TRENCH ORIENTATION : N-S



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LOG OF TRENCH MS-T-4 MULESHOE VALLEY, NEVADA

30 JUN 81

FIGURE 1574

BULK SAMPLE	EPTH	LITHOLOGY	NSCS	CONSISTENCY	SOIL DESCRIPTION	REMARKS	AN	IEV LYS	15	11	ī
0	2 -		SW- SM	dense	GRAVELLY SAND, brown, fine to coarse, well graded; slightly moist, angular, calcareous; some fine angular gravel; trace nonplastic silt; occasional cobbles to 6" size; stage II caliche (0.5' - 6.0').	vertical wells stable		59			
	8 -			very dense							
- 2	•				TOTAL DEPTH 6.0' (1.8m)	cementation at 6,0' exceeded capacity of Case 580C backhoe					
-3	10-										
-4	12-										
	14-										
- 5	18-										
	18-										
-6	20-									'	

SURFACE ELEVATION : 5700' (1737m)
DATE EXCAVATED : 30 October 1979

SURFICIAL GEOLOGIC UNIT: A51
TRENCH LENGTH : 8.0° (2.4m)
TRENCH ORIENTATION : E-W



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LOG OF TRENCH MS-T-5 MULESHOE VALLEY, NEVADA

30 JUN 81

FIGURE 13-7-6

BULK SAMPLE	PTH	L.1 THO LOBY	nscs	CONSISTENCY	SOIL DESCRIPTION	REMA	ARKS	AN	IEV LYS	15] 1	ءَ ۾
- 1	0 2 - 4 - 8 -		SM	medium dense	interbedded layers of SILTY SAND and GRAVELLY SAND: GRAVELLY SAND (SW-SM): light brown, fine to coarse, well graded, slightly moist, subangular, calcareous; some fine gravel; trace nonplestic silt; stage I caliche. SILTY SAND (SM): light brown, fine to coarse, poorly graded, slightly moist, subangular, calcareous; some nonplestic silt; little fine gravel; stage I caliche (12.0' - 14.0').		al walls		51			
	10-		SW- SM	dense	•			21	72	7		
-4	14-		SM	dense	TOTAL DEPTH 14,0' (4.3m)		,					
-5	16-											
	16-											
- 6	20-											

SURFACE ELEVATION : 5360' (1634m)
DATE EXCAVATED : 31 October 1979

SURFICIAL REGLOSIS UNIT: A51
TRENCH LENGTH : 16.0' (4.9m)
TRENCH ORIENTATION : E-W



MX SITING INVESTIGATION
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LOG OF TRENCH MS-T-8
MULESHOE VALLEY, NEVADA

30 JUN 81

FIGURE 13-7-6

DULK SAMPLE	WETERS S	FEET #	LITHOLOGY	USCS	CONSI STENCY	SOIL DESCRIPTION	REMARKS	AN	IEV ALY:		LL	PI
	0	2		GM	dense	SANDY GRAVEL, light brown, fine to coerse, poorly graded, slightly moist, angular, calcareous; some fine to coerse sand; little nonplastic silt; stage III caliche (2.0' - 3.0').	vertical wells			14		
	- 1	4-				TOTAL DEPTH 3.0' (0.9m)	comentation at 3.0' exceeded capacity of Case 580C baskhoe					
	- 2	8-								<u>.</u>		
	Ī	8							-			
	- 3	10-										
	-4	12-										
		14-							 			
	- 5	18-										
ļ		18-										
	- 6	20-										

SURFACE ELEVATION : 5630' (1716m)
DATE EXCAVATED : 30 October 1979

SURFICIAL GEOLOGIC UNIT: ASI

TRENCH LENGTH : 7.0' (2.1m)

TRENCH ORIENTATION : E-W



MX SITING INVESTIGATION
DEPARTMENT OF THE AIR FORCE
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LOG OF TRENCH MS-T-7 MULESHOE VALLEY, NEVADA

30 JUN 81

FIGURE 11-7-7

BULK SANPLE	METERS 33	PTH 133	LITHOLOGY	nscs	Cons) stency	SOIL DESCRIPTION	REMARKS	AN	IEV LYS	15	LL	PI
	0	2~		GC	dense	CLAYEY GRAVEL, brown, fine to coarse, poorly graded, dry, angular to subangular, calcareous; some slightly plastic clay; some fine to coarse send; stage II caliche (0.5' - 2.0') stage IV caliche at 2.5'.	vertical walls state		26			
	- 1	4-				TOTAL DEPTH 2.5' (0.8m)	comentation et 2.5' exceeded capacity of Case 580C backhoe					
i	- 2	8 -						; ; ;				
		6 -										
	_ 3	10-										
	-4	12-										
		14-										
	- 5	16-										
	- 8	18-										
		20-										

SURFACE ELEVATION : 5060' (1700m)

DATE EXCAVATED : 1 November 1979

SURFICIAL SEGLOCIC UNIT: A51
TRENCH LENGTH : 6.0' (1.8m)
TRENCH ORIENTATION : E-W



MX SITING INVESTIGATION
DEPARTMENT OF THE AIR FORCE
BMO/AFRCE-MX

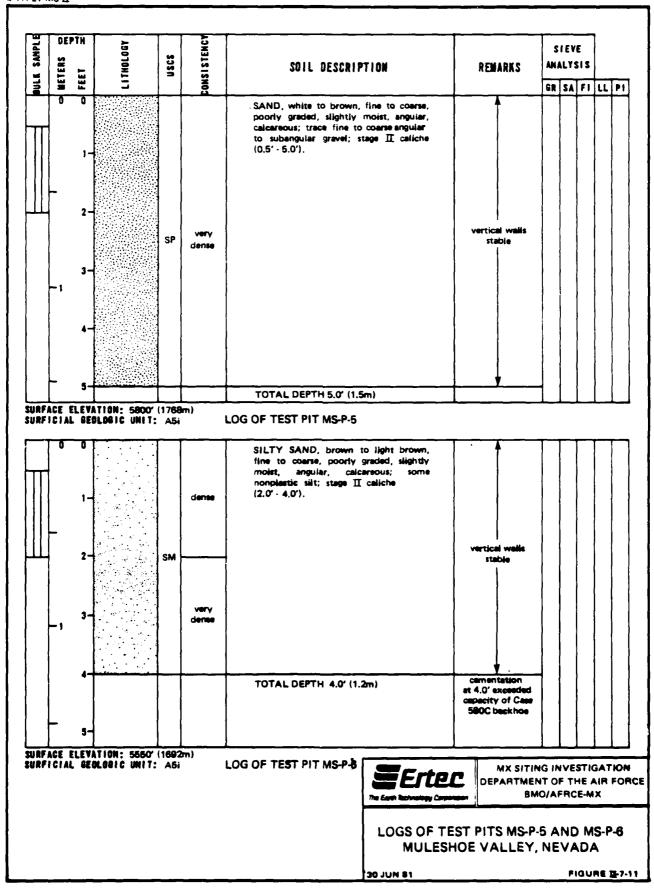
LOG OF TRENCH MS-T-8
MÜLESHOE VALLEY, NEVADA

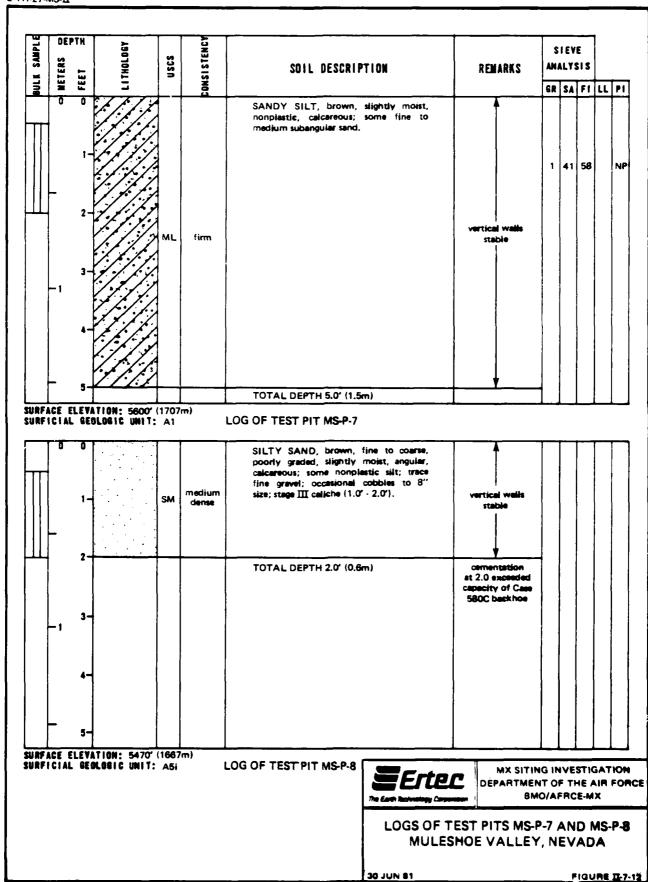
18 MUL 0E

FIGURE II-7-8

SAMPL		TH	LITHOLOGY	USCS	ONSISTENCY	SOIL DESCRIPTION	REMARKS	1	IEV ALY:			
3	METERS	FEET		3	ISMO	out organii iian	"CZARKO	40	e a	Fi		Ter
	0	0		CL	firm	SILTY CLAY, dark brown to white, dry to slightly moist, slightly plastic, calcareous; trace fine to medium subangular to subrounded sand; occasional boulders to 20" size; stage III - IV caliche	vertical walls					
!	 -	2-			hard	(1.0' - 2.0').	stable					
		3-				TOTAL DEPTH 2.0' (0.6m)	cementation at 2.0' exceeded capacity of Case 580C backhoe					
	-1	4-										
		5-										
RF/	ACE E	LEV	ATION: 6500'(1981	m)		<u> </u>	ــــــــــــــــــــــــــــــــــــــ	L	<u> </u>	<u> </u>	_
RF	I C I AL	SE	DLOGIC UNIT:	A5o	` ' ''	LOG OF TEST PIT MS-P-3						
	0	1-				GRAVELLY SAND, brown, fine to coarse, well graded, dry, angular, calcareous; some fine to coarse gravel; trace nonolectic sitt; stage I - II caliche (0.5' - 5.0').		28	67	5		
	_			SW- SM	dense	coarse, well graded, dry, angular, calcare- ous; some fine to coarse gravel; trace nonplestic silt; stage I - II caliche	vertical wells stable	28	67	5		
	-1	2-			dense	coarse, well graded, dry, angular, calcare- ous; some fine to coarse gravel; trace nonplestic silt; stage I - II caliche		28	67	5		
	-1				dense	coarse, well graded, dry, angular, calcare- ous; some fine to coarse gravel; trace nonplestic silt; stage I - II caliche		28	67	5		
	-1				dense	coarse, well graded, dry, angular, calcare- ous; some fine to coarse gravel; trace nonplestic silt; stage I - II caliche		28	67	5		
I RF	1	3- 4- 5-	ATION: 5820'(DLOBIC UNIT:	SM	ni	coarse, well graded, dry, angular, calcareous; some fine to coarse gravel; trace nonolestic sit; stage I - II caliche (0.5' - 5.0').	MX SITIN DEPARTMEN	GIN	VE:	STIC	IA.	

¥





SIEVE ANALYSIS

60 31 9

GR SA FI LL PI

POPICIAL GEOLOGIC UNIT: LOG OF TEST PI



MX SITING INVESTIGATION DEPARTMENT OF THE AIR FORCE BMO/AFRCE-MX

LOG OF TEST PIT MS-P-9 MULESHOE VALLEY, NEVADA

30 JUN 81

FIGURE IL-7-13

ACTIVITY	GROUND SURFACE ELEVATION, FEET		DE PTH, FEET	uscs	SOIL DESCRIPTION	1 1	IEV ALY:	_		
	(METERS)	UNIT	(METERS)			8R	SA	FI	ιL	P
MS-CS-5	6080 (1853)	A5i	0.0 - 0.5 (0.0 - 0.2)	GC	CLAYEY GRAVEL, dark brown, fine to coarse, poorly graded, subangular to sub-rounded, calcareous; some slightly plastic clay; little fine to coarse sand.	46	19	35	33	12
			0.5 - 1.0 (0.2 - 0.3)	GP	SAN DY GRAVEL, white, fine to coarse, poorly graded, subangular to subrounded, calvareous; little fine to coarse sand; some cobbles to 10° size; stage IV caliche (0.5° - 1.0°).					
MS-CS-8	5960 (1817)	A5o	0.0 - 2.0 (0.0 - 0.6)	SM	GRAVELLY SAND, light brown, fine to coarse, poorly graded, angular, calcareous; some fine to coarse gravel; little nonplastic silt; stage II - III caliche (0.5' - 2.0').		[
MS-CS-10	5690 (1734)	A5i	0.0 - 2.0 (0.0 - 0.6)	ML	SILT, brown, slightly plastic, calcareous; trace fine subengular sand.		Į			
MS-CS-12	5510 (1679)	A5i	0.0 - 4.0 (0.0 - 1.2)	GM	SANDY GRAVEL, light brown, fine, poorly graded, subangular, calcareous; some fine to coarse sand; some nonplactic to slightly plastic silt; boulder to 24" size at 2.5".	38	31	31		
MS-CS-13	6000 (18 29)	A5i	0.0 - 2.0 (0.0 - 0.6)	SM	SILTY SAND, brown, fine to coarse, poorly graded, engular, calcareous; some nonplastic silt.					
MS-CS-18	57 40 (1750)	A5 i	0.0 - 2.0 (0.0 - 0.6)	SM	SILTY SAND, light brown, fine to course, poorly graded, angular to sub-angular, calcareous; some nonplastic to slightly plastic silt; occasional cobbles to 7" size.					
MS-CS-20	5450 (1661)	A5y	0.0 - 2.0 (0.0 - 0.6)	ML	SANDY SILT, light brown, nonplastic, calcareous; little fine subangular sand.	0	18	82		2
мѕ-сѕ-23	5400 (1646)	A5i	0.0 - 2.0 (0.0 - 0.6)	SM	SILTY SAND, light brown, fine to coarse, poorly graded, subangular, calcareous; little nonplastic silt.			}		



LOGS OF SURFICIAL SOIL SAMPLES MULESHOE VALLEY, NEVADA

30 JUN 81

FIGURE IT-1

8.0 SURFICIAL SOIL SAMPLE LOGS

Explanation: Finalized logs of the surficial samples are
presented in this section. Explanations of the column headings
on the logs follow:

A. Designations - Surficial samples are identified as follows:

MS-CS-1

- MS abbreviation for the valley (e.g., MS-Muleshoe)
- CS abbreviation for surficial sample
 - 1 number of activity
- B. Ground Surface Elevation Indicated elevations on the logs are estimated from topographic maps of the study area within an accuracy of half the contour interval.
- C. Surficial Geologic Unit Indicates the surficial geologic unit in which the activity is located.
- D. Depth Indicates depth interval for which soil description is given.
- E. USCS Unified Soil Classification Symbol; see Table II-6-1 of Section 6.0, "Borings Logs," for details of USCS.
- F. Soil Description Soil is described based on field visual descriptions and/or laboratory test results. See Section 6.0, "Boring Logs," for procedures of soil description.
- G. Sieve Analysis, LL and PI These are from results of laboratory tests. See Section 6.0, "Boring Logs," for explanation.

9.0 LABORATORY TEST RESULTS

Explanation: Laboratory test results are presented in this section. Table II-9-1 contains a summary of laboratory test results. This table shows results of sieve analysis; plasticity data; in-situ dry unit weight, moisture content, degree of saturation, and void ratio for drive and Pitcher samples; results of compaction tests; and specific gravity of solids. Other tests such as triaxial compression, unconfined compression, direct shear, consolidation, chemical, and California Bearing Ratio (CBR) are indicated on the table. Tables II-9-2 through II-9-6 and Figures II-9-1 through II-9-3 present results of triaxial compression, unconfined compression, direct shear, consolidation, chemical, and CBR tests.

All tests were performed in general accordance with the American Society for Testing and Materials (ASTM) procedures. The following list presents the ASTM designations for the tests performed during the investigation.

Type of Test	ASTM	Designations
Particle Size Analysis	D	422-63
Liquid Limit	D	423-66
Plastic Limit	D	424-59
Unit Weight	D	2937-71
Moisture Content	D	2216-71
Compaction	D	1557-70
Specific Gravity of Solids	D	854-58
Triaxial	D	2850-70
Unconfined Compression	D	2166-66
Direct Shear	D	3080-72
Consolidation	D	2435-70
Test for Alkalinity (pH)	D	1067-70
Water Soluble Sodium	D	1428-64
Water Soluble Chloride	D	512-67
Water Soluble Sulphate	D	516-68
Water Soluble Calcium	D	511-72
Calcium Carbonate	D	1126-67
California Bearing Ratio (CBR)	D	1883-73

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Explanation for the tables and figures presented in this section are as follows.

- A. Activity Number Boring, trench, test pit, or surface sample designation.
- B. Sample Number Prefix indicates the type of sample; explanation is at the bottom of the table.
- C. Sample Interval This is the depth range measured from ground surface over which the sample was obtained.
- D. Percent Finer by Weight Presents the results of laboratory particle size analysis (ASTM D 422-63) performed on representative soil samples at the depth indicated. The numbers represent the percent (by dry weight) of the total sample weight passing through each sieve size indicated.
- E. Atterberg Limits (ASTM D 423-66 and D 424-59)
 - LL Liquid Limit, the water content (as percent of soil dry weight) corresponding to the arbitrary limit between the liquid and plastic states of consistency of a soil (ASTM D 423-66).
 - PL Plastic Limit, the water content corresponding to an arbitrary limit between the plastic and the semisolid state of consistency of a soil (ASTM D 424-59).
 - PI Plasticity Index, numerical difference between the liquid limit (LL) and the plastic limit (PL) indicating the range of moisture content within which a soil-water mixture is plastic.
 - NP Nonplastic.

- F. USCS Unified Soil Classification Symbols are given here; see Table II-6-1 in Section 6.0, "Boring Logs," for complete details of USCS system.
- G. In Situ Presents results of tests on drive and Pitcher samples.
 - Dry Unit Weight Indicates dry unit weight of soil determined as per ASTM D 2937-71.
 - Moisture Content Weight of water reported in percent of dry weight of soil sample (ASTM D 2216-71).
 - Saturation The degree of saturation in a soil sample is defined as the ratio (in percent) of the volume of water to the volume of all voids in the soil.
 - Void Ratio The numerical ratio of the volume of voids to the volume of solids in a soil specimen.
- H. Compacted Indicates results of laboratory maximum dry density and optimum moisture content test as per ASTM D 1557-70.
- I. Specific Gravity of Solids (ASTM D 854-58) Indicates the ratio of 1) the weight in air of a given volume of soil solids at a stated temperature, to 2) the weight in air of an equal volume of distilled water at a stated temperature.
- J. Triaxial The triaxial compression tests were performed in accordance with the procedures of ASTM D 2850-70. The following explanations and definitions apply.

Triaxial Compression Test - A cylindrical specimen of soil is surrounded
by a fluid in a pressure chamber and subjected to an isotropic pressure. An additional compressive load is then applied,
directed along the axis of the specimen
called the axial load.

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Consolidated-Drained (CD) Test

- A triaxial compression test in which the soil was first consolidated under an allaround confining stress (test chamber pressure) and was then compressed (and hence sheared) by increasing the vertical stress. "Drained" indicates that excess pore water pressure generated by strains are permitted to dissipate by the free movement of pore water during consolidation and compression.

Consolidated-Undrained (CU)

Test

- A triaxial compression test in which essentially complete consolidation under the confining (chamber) pressure is followed by a shear test at constant water content.

Confining Pressure

(₀3)

- The isotropic chamber pressure applied to the soil specimen during consolidation and compression.

Maximum Deviator

Stress

(01-03)

- The difference between the major and minor principal stresses in the specimen at failure. The major principal stress on the specimen is equal to the unit axial load plus the chamber pressure and the minor principal stress on the specimen is equal to the chamber pressure.
- Strain Rate Axial strain, ϵ , at a given stress level is defined as the ratio of the change in length (Δ L) of the specimen to the original length of the specimen (L_0). The rate of strain was controlled during the test so that this ratio increased at equal increments for each minute of testing.
- Back Pressure Pressure in excess of atmospheric applied to the pore water of a soil sample. Back pressure is usually applied to (1) increase saturation of the sample, or (2) simulate the actual in-situ pressure regime.
- K. Unconfined Compression Test procedures were as described in ASTM D 2166-66. Unconfined compressive strength is

defined as the load per unit area at which an unconfined prismatic or cylindrical specimen of soil will fail in a simple compression test. In these methods, unconfined compressive strength is taken as the maximum load attained per unit area or the load per unit area at 20 percent axial strain, whichever occurred first during the performance of a test.

- L. Direct Shear The procedures of ASTM D 3080-72 were followed for direct shear testing. In this test, soil under an applied normal load is stressed to failure by moving one section of the soil container (shear box) relative to the other section. Normal stress is the value of load per unit area acting perpendicular to the plane of shearing. Maximum shear strength is defined as the maximum resistance (ksf) of a soil to shearing (tangential) stresses.
- M. Consolidation (ASTM D 2435-70) A consolidation test is a test in which a cylindrical soil specimen is laterally confined in a ring and compressed between porous plates. The term "consolidation," as used here, indicates the gradual reduction in volume of the soil mass resulting from an increase in compressive stress (axial load per unit area).
- N. Chemical The chemical tests performed on soil samples included: pH; water soluble sodium, chloride, sulphate, calcium; and calcium carbonate content. pH is an index of

the acidity or alkalinity of a soil in terms of the logarithm of the reciprocal of the hydrogen ion concentration.

ASTM test procedure designations for these chemical tests are included in the list on the first page of these Explanations.

O. CBR - California Bearing Ratio (CBR) is the ratio (in percent) of the resistance to penetration developed by a subgrade soil to that developed by a standard crushed-rock base material. The procedures for conducting a CBR test were as outlined in ASTM D 1883-73. The materials tested for CBR were also analyzed for particle-size distribution (ASTM D 422-63) and compaction characteristics (ASTM D 1557-70). The term "percentage of maximum density" indicates the ratio (as a percentage) of the compacted sample dry unit weight to maximum dry density obtained in the laboratory from ASTM D 1557-70, "Moisture-Density Relations of Soils Using 10-pound (4.5-kg) Hammer and 18-inch (457-mm) Drop."

			1					PERCEI	T FIN	R BY V	EISHT					
Ė	<u> </u>	SAMPLE I	NTERVAL		S	TANDARI	SIEV	E OPEN	ING		U S	STAN	DARD S	IEVE N	10.	PARTI SIZE
ACT I VI TY Number	SAMPLE Number			BLDRS	COBI	BLES		GRA	VEL			SA	ND		\$11	T OR CL
2 2	중로	FEET	METERS	24"	12"	6"	3"	15"	3/4"	3/8"	4	10	40	100	200	. 005
MS-B-1	P-1	0.8 - 1.6	0.24 - 0.49													
	P-1	1.6 - 2.4	0.49 - 0.73										100	97_	93	
	P-2	3,0 - 3,8	0.91 - 1.16									100	97	93	85	
	D-3	6,8 - 7,3	2.07 - 2.23					100	97	91	_86	81	70	48	36	
	D-4	10.5 - 11.0	3.20 - 3.35													
	D-5	15.5 - 16.0	4.72 - 4.88			L			<u> </u>	100	99	96	39	16	13	
	P-6	20.0 - 20.9	6.10 - 6.37			<u></u>	<u> </u>					100	86	36	22	
	P-7	25.0 - 25.8	7.62 - 7.86						<u> </u>					L		
i	P-8	30.5 - 31.0	9.30 - 9.45									L		<u> </u>		L
Ĺ	P-8	31.2 - 31.7	9.51 - 9.66	<u> </u>											<u> </u>	
L	P-8	31.9 - 32.4	9.72 - 9.86			L	L		100	99	95	86	68	37	22	↓ ↓
	P-9	40.0 - 40.6	12.19 - 12.37			<u> </u>	L		<u> </u>	L	L		 	<u> </u>	<u> </u>	
Ĺ	P-10	50.0 - 52.4	15,24 - 15,97	L					L		100	98	79	58	51	
<u> </u>	P-11	60.8 - 61.6	18.53 - 18.78						L		100	88	35	15	11	L
	P-12	70.8 - 71.6	21.58 - 21.82			<u> </u>	L		L					L		1
	P-13	80.0 - 80.9	24.38 - 24.66				L		100	99	96	90	42	15	10	
	P-14	90.8 - 91.2	27.68 - 27.80	1		<u> </u>		<u> </u>	<u> </u>		100	97	65	41	29	
	P-15	98.8 - 99.6	30.11 - 30.36	↓					!		100	97	74	48	34	
MS-B-2	P-1	0.8 - 1.7	0.24 - 0.52	 	 	 		100	93	90	82	75	65	50	38	
1.000	D-3	5.5 - 6.0	1.68 - 1.83	 		 	 		35	50	- UE	- ''	1	 "		
t	D-4	8.5 - 9.0	2.59 - 2.74	 		 	 	— —	 		 	 	 	 	 	1
 	D-5	11.0 - 11.5	3.35 - 3.51	╂		 	}	100	94	75	55	36	13	8	6	1
	D-6	15.5 - 16.0	4.72 - 4.88	1		 	├ ┈──	100	1 37	100	99	97	91	75	58	1
	D-6	15.5 - 16.0	4.72 - 4.88	 		 	 	 	 	100			 	 '``	1	1
	D-7	20.5 - 21.0	6,25 - 6,40	 	 -	 -	 					├──	 	 	 	1
	D-8	25.3 - 25.8	7,71 - 7,86	 		 	 	100	95	73	50	35	23	14	11	
 	D-9	31.0 - 31.5	9.45 - 9.60	1		 	 		1-55	100	90	61	19	5	3	
<u> </u>	D-10	40.2 - 40.7	12,25 - 12,41	 		 	100	75	57	43	1 3	24	11	6	5	
	D-11	50.2 - 50.7	15.30 - 15.45	-	 -	 	1 100	- " -	 ~	 	 		 ``	ऻ ⊸ॕ─	├	
 	D-12	60.2 - 60.7	18.35 - 18.50	1	 	 	 		 	 	100	98	62	31	21	
	D-13	70.3 - 70.8	21,43 - 21,58	1	 -	1	 	 	100	89	76	58	22	12	8	
	D-14	80.2 - 80.7	24.44 - 24.60	1		1	T		T	<u> </u>	<u> </u>		T	T -	T -	
	D-15	90.3 - 90.8	27.52 - 27.68	1		<u> </u>	1		100	96	83	75	49	28	17	
	D-16	99.2 - 99.7	30.24 - 30.39								100	96	72	37	18	
	 										<u> </u>		 	 	 	
MS-B-3	D-1	1.0 - 1.5	0.30 - 0.46	!	L			L	100	93	84	69	35	18	13	
}	D-2	3.5 - 4.0	1.07 - 1.22	-		 	<u> </u>	<u> </u>	 	100	96	62	16	6	3	
}	D-3	6.0 - 6.5	1.83 - 1.98	}	<u> </u>	└	ļ	L	 				├	 	├ ─	∤
<u> </u>	D4	8.5 - 9.0	2.59 - 2.74			L	<u> </u>	ļ	L	<u> </u>	L		<u> </u>	ļ.,,	_	
<u> </u>	D-5	10.5 - 11.0	3.20 - 3.35			├ ──	↓	100	92	91	89	81	48	29	24	
	D-6	15.3 · 15.8	4.66 - 4.82	1	ļ		 	 	100			 	27	 _ -	 _	 -
L	D-7	21.0 - 21.5	6,40 - 6,55	1	L	1	<u>i</u>	<u> </u>	100	99	96	88	27	9	7	1

NOTES:

(a) Sample types

(c) USCS - Unified Soil Classification System

35 - Standard split spoon

P - Pitcher

D - Fugro Drive

(d) * Indicates that test has been performed and results are included in this report

8,b - Bulk

(b) MP - Not Plastic

RD SIEVE NO. PARTICLE SIZE (mm) SILT OR CLAY					1	
CL 73.3 1174 10.4 21.9 1.26	ر الا	. s	IL (d)	SIG		E S
CL 73.3 1174 10.4 21.9 1.26	SPECIFIC GRAVITY OF SOLIDS		TRIAXIAL	UNCONFINED Compression	DIRECT	CONSOLIDATION
CL 73.3 1174 10.4 21.9 1.26	S S S	22.	IRI		2 × 3	SES
00 97 93 33 18 15 CL 72.6 1163 10.7 22.2 1.28 97 93 85 31 20 11 CL 75.4 1208 11.4 24.8 1.24 70 48 36 NP SM 97.3 1559 7.3 26.9 0.73 39 16 13 NP SM 108.1 1732 7.2 34.7 0.56 39 16 13 NP SM 106.9 1712 8.2 37.1 0.61 86 36 22 SM 88.9 1424 13.6 41.0 0.90 8 39 1424 13.6 41.0 0.90 0.90 8 37 22 22 19 3 SM 103.6 1660 12.4 53.5 0.63 9 5 5 5 5 5 3 10.0 <td< th=""><th></th><th></th><th></th><th></th><th></th><th>_=</th></td<>						_=
97 93 85 31 20 11 CL 75.4 1208 11.4 24.8 1.24 70 48 36	2.65	265		-		
70 48 36 NP SM 97.3 1559 7.3 26.9 0.73 39 16 13 NP SM 106.9 1712 8.2 37.1 0.61 86 36 22 SM 106.9 1712 8.2 37.1 0.61 SM 106.9 1712 8.2 37.1 0.61 0.90 SM 109.7 1757 9.9 49.8 0.54 SM 103.6 1660 12.4 53.5 0.63 SM 103.8 1663 10.5 45.5 0.62 68 37 22 22 19 3 SM 106.7 1709 10.0 46.4 0.58 SM 111.1 1780 9.2 48.2 0.52 0.52 79 58 51 NP ML 96.7 1549 19.3 70.1 0.74 35 15 11 SW-SM 111.0 1778 11.7 61.2 0.52 42 15	-2.00					
39 16 13 NP SM 108.1 1732 7.2 34.7 0.56 86 36 22 SM 106.9 1712 8.2 37.1 0.61 SM 38.9 1424 13.6 41.0 0.90 SM 109.7 1757 9.9 49.8 0.54 SM 103.6 1660 12.4 53.5 0.63 SM 103.8 1663 10.5 45.5 0.62 68 37 22 22 19 3 SM 106.7 1709 10.0 46.4 0.58 SM 111.1 1780 9.2 48.2 0.52 0.52 79 58 51 NP ML 96.7 1549 19.3 70.1 0.74 35 15 11 SW-SM 111.0 1778 11.7 61.2 0.52 42 15 10 SW-SM 117.7 1885 15.6 97.9 0.43 65 41 29 SM			 -			
39 16 13 NP SM 106.9 1712 8.2 37.1 0.61 0.61 86 36 22 SM 88.9 1424 13.6 41.0 0.90 SM 109.7 1757 9.9 49.8 0.54 SM 103.6 1660 12.4 53.5 0.63 SM 103.8 1663 10.5 45.5 0.62 68 37 22 22 19 3 SM 106.7 1709 10.0 46.4 0.58 SM 111.1 1780 9.2 48.2 0.52 79 58 51 NP ML 96.7 1549 19.3 70.1 0.74 35 15 11 SW-SM 111.0 1778 11.7 61.2 0.52 42 15 10 SW-SM 117.7 1885 15.6 97.9 0.43 65 41 29 SM 121.1 1940 7.6 52.8 0.39						
86 36 22 SM 88.9 1424 13.6 41.0 0.90 SM 109.7 1757 9.9 49.8 0.54 SM 103.6 1660 12.4 53.5 0.63 SM 103.8 1663 10.5 45.5 0.62 68 37 22 22 19 3 SM 106.7 1709 10.0 46.4 0.58 SM 111.1 1780 9.2 48.2 0.52 79 58 51 NP ML 96.7 1549 19.3 70.1 0.74 35 15 11 SW-SM 111.0 1778 11.7 61.2 0.52 42 15 10 SW-SM 117.7 1885 15.6 97.9 0.43 65 41 29 SM 121.1 1940 7.6 52.8 0.39	2,76	2.76			•	
SM 109.7 1757 9.9 49.8 0.54 SM 103.6 1660 12.4 53.5 0.63 SM 103.8 1663 10.5 45.5 0.62 68 37 22 22 19 3 SM 106.7 1709 10.0 46.4 0.58 SM 111.1 1780 9.2 48.2 0.52 79 58 51 NP ML 96.7 1549 19.3 70.1 0.74 35 15 11 SW-SM 111.0 1778 11.7 61.2 0.52 SM 111.1 1780 11.8 61.8 0.52 42 15 10 SW-SM 117.7 1885 15.6 97.9 0.43 65 41 29 SM 121.1 1940 7.6 52.8 0.39						
SM 103.6 1660 12.4 53.5 0.63 SM 103.8 1663 10.5 45.5 0.62 SM 106.7 1709 10.0 46.4 0.58 SM 111.1 1780 9.2 48.2 0.52 NP ML 96.7 1549 19.3 70.1 0.74 SW-SM 111.0 1778 11.7 61.2 0.52 SM 111.1 1780 11.8 61.8 0.52 SM 111.1 1780 11.8 61.8 0.52 SW-SM 117.7 1885 15.6 97.9 0.43 SM 121.1 1940 7.6 52.8 0.39						
68 37 22 19 3 SM 106.7 1709 10.0 46.4 0.58 79 58 51 NP ML 96.7 1549 19.3 70.1 0.74 35 15 11 SW-SM 111.0 1778 11.7 61.2 0.52 SM 111.1 1780 11.8 61.8 0.52 42 15 10 SW-SM 117.7 1885 15.6 97.9 0.43 65 41 29 SM 121.1 1940 7.6 52.8 0.39			•			
68 37 22 19 3 SM 106.7 1709 10.0 46.4 0.58 .79 58 51 SM 111.1 1780 9.2 48.2 0.52 .79 58 51 NP ML 96.7 1549 19.3 70.1 0.74 35 15 11 SW-SM 111.0 1778 11.7 61.2 0.52 SM 111.1 1780 11.8 61.8 0.52 42 15 10 SW-SM 117.7 1885 15.6 97.9 0.43 65 41 29 SM 121.1 1940 7.6 52.8 0.39			•			
SM 111.1 1780 9.2 48.2 0.52 79 58 51 NP ML 96.7 1549 19.3 70.1 0.74 35 15 11 SW-SM 111.0 1778 11.7 61.2 0.52 SM 111.1 1780 11.8 61.8 0.52 42 15 10 SW-SM 117.7 1885 15.6 97.9 0.43 65 41 29 SM 121.1 1940 7.6 52.8 0.39						
35 15 11 SW-SM 111.0 1778 11.7 61.2 0.52 SM 111.1 1780 11.8 61.8 0.52 42 15 10 SW-SM 117.7 1885 15.6 97.9 0,43 65 41 29 SM 121.1 1940 7.6 52.8 0.39						\sqsubseteq
SM 111.1 1780 11.8 61.8 0.52 42 15 10 SW-SM 117.7 1885 15.6 97.9 0.43 65 41 29 SM 121.1 1940 7.6 52.8 0.39						
42 15 10 SW-SM 117.7 1885 15.6 97.9 0,43 65 41 29 SM 121.1 1940 7.6 52.8 0.39			<u> </u>	L		
65 41 29 SM 121.1 1940 7.6 52.8 0.39				<u> </u>		
<u> </u>				<u> </u>		L
74 48 34 SM 103.4 1656 17.8 76.3 Q.63			<u> </u>	<u> </u>		L
			.	}		-
			ļ	 		
65 50 38 NP SM 105,4 1688 3.4 15,4 0.60			 		ļ	
SM 102.0 1634 5.1 21.0 0.65				├		
NP SM 103.3 1655 5.5 23.3 0.63				├		
13 8 6 NP SW-SM 114.5 1834 6.7 38.1 0.47			!	 		
91 75 58 NP ML 96.1 1540 6.8 24.4 0.75				├	 	
ML 91.8 1471 8.8 28.4 0.84			 	} -	 -	-
SM 102.3 1639 9.9 41.6 0.65			├ ──	┼	├ ~──	
23 14 11 GP-GM 115.4 1849 12.4 72.6 0.46 SW 112.8 1807 8.7 47.5 0.49			 	∤		
			 	┼	 	 -
11 6 5 GW-GM 120.1 1924 10.8 72.5 0.40	 		 	┼~~~	 	 -
SM 100.1 1603 13.8 54.5 0.68 62 31 21 SM 101.2 1621 12.0 48.6 0.67			 	 	 	
22 12 8 SW-SM 119.3 1911 9.5 62,6 0.41	 		 	1	 	<u> </u>
SM 99.8 1599 19.0 74.5 0.69			T	1		
49 28 17 NP SM 104.9 1680 22.0 97.9 0.61	1		1	T		
72 37 18 SM 96.8 1551 26.9 97.9 0.74	1		T	1		
			T	Ţ	<u> </u>	Γ
35 18 13 NP SM 100.9 1616 9.1 36.6 0.67						
16 6 3 SW 104.5 1674 4.2 18.5 0.61			T	1		
SW 90.7 1453 11.7 36.7 0.86						
SW 117.8 1887 6.2 39.2 0.43			Π			
48 29 24 31 18 13 SC 104.8 1679 13.6 60.6 0.61						Γ
SM 115.3 1847 8.3 48.3 0.46						T .
27 9 7 SP-SM 105.6 1692 7.8 35.5 0.60			<u> </u>		<u> </u>	┺-

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SUMMARY OF LABC MULESHOE VA PAGE 1

30 JUN 81

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Ł												
				OMPACTE	0		€	6.8		3		}
	5		MAX	MUM	15 A	7 C	=	SS		DAT	=	
F	SATURATION (\$)	VOIO RATIO	DRY DE		OPTIMUM Moisture (%)	SPECIFIC GRAVITY OF SOLIDS	TRIAXIAL (d)	UNCONFINED COMPRESSION	DIRECT	CONSOLIDATION	CHEMICAL	_
٢	SAT	S.A.	(pcf)	(kg/m³)	89	SPE OF	Ξ	35	吕罴	Sies	E	<u>چ</u>
	21.9	1.26								<u> </u>		
F	22.2	1.28				2.65	 				 	
	24.8	1.24					<u> </u>					
	26.9	0.73										
L	34.7	0.56	ļ									
L	37.1	0.61	<u> </u>			2.76						L
<u> </u>	41.0	0.90					ļ				*	L I
\vdash	49.8	0.54				L	L	 _				
	53.5 45.5	0.63 0.62		 	 		<u> </u>	 -			 	
K -	46.4	0.62		 	 		+	 				├
F	48.2	0.52	<u> </u>		 							
3	70.1	0.74						-				
7	61,2	0.52										
8	61.8	0.52										
8_6	97.9	0.43										
	52,8	0.39										
8	76.3	0.63										
_	<u> </u>											
4	15.4	0.60		ļ			L	L			L	
1	21.0	0.65		<u> </u>			L	• •			*	
5	23,3	0.63					ļ	 				<u> </u>
7	38.1	0.47					 	 				
8 8	24.4 28.4	0.75 0.84				<u> </u>		 	<u> </u>	<u> </u>	ļ	
9	41.6	0.65			<u> </u>					*		
.4	72.6	0.46	 				 -					
7	47.5	0.49				<u>-</u>		 				
.8	72.5	0.40										
.8	54.5	0.68		<u> </u>							 	
.0	48.6	0.67										
5	62.6	0.41										
.0	74.5	0.69										
.0	97.9	0.61					L					
.9	97.9	0.74					<u> </u>					
					ļ							
.1	36.6	0.67			 			 				
.2	18.5	0.61				 		 			L	
.7	36.7	0.86			 						 	
.2	39.2	0.43			 			 			 	├
.6 .3	60.6 48.3	0.61		ļ								
8	35,5	0. 46 0. 60			 			} -				
<u></u> _	30,0	0.00			ليسيا			<u> </u>				ليبيسا



SUMMARY OF LABORATORY RESULTS **MULESHOE VALLEY, NEVADA** PAGE 1 OF 2

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	^			1					PERCE	NT FINE	R BY W	ELGHT				
1 T.Y	R (a)	SAMPLE	NTERVAL		S	TANDARO	SIEV	E OPEN	ING		U S	STAN	DARD S	IEVE N	10 .	SI
ACT I V I TY Number	SAMPLE			BLDRS	COBE	BLES		GRA	VEL			SA	ND		\$11	LT O
AC NU	중골	FEET	METERS	24"	12"	6"	3"	1½"	3/4"	3/8"	4	10	40	100	200	.00
MS-B-3	D-8	25.2 - 25.7	7.68 - 7.83`						100	97	94	88	64	37	25	П
	D-9	30.2 - 30.7	9.20 - 9.36					100	99	93	85	70	36	19	13	
	D-10	40.5 - 41.0	12.34 - 12.50							100	97	89	57	28	18	
	P-11	50.8 - 51.6	15.24 - 15.48						100	91	77	66	38	18	12	\Box
	P-12	60,2 - 60.7	18.35 - 18.50													<u> </u>
	P-12	60.2 - 60.7	18.35 - 18.50		<u> </u>			L								<u> </u>
	P-12	61.0 - 61.5	18.59 - 18.75						<u> </u>						<u> </u>	<u> </u>
	P-12	61.8 - 62.3	18.84 - 18.99						<u> </u>		100	99	88	6.2	40	1
	P-13	70.7 - 70.7	21.34 - 21.55			<u> </u>		L	<u> </u>		100	94	69	42	26	
	P-14	86.8 - 87.6	26.46 - 26.70						L						<u> </u>	<u></u>
	'P-15	98.8 - 99.8	30.11 - 30.42	-	ļ				├		100	84	30	14	10	├
MS-T-1	B-1	0.5 - 2.0	0.15 - 0.61						100	98	98	96	89	81	72	上
140 T O		05 00	0.15 0.01	-	 	 -	 -	ļ		 -	100			1 20	21	├ ─
MS-T-2	B-1	0.5 - 2.0	0.15 - 0.61	+	├──-				├ ──	100	100	95	65	39	31	┼
	b-2	5.0 - 6.0	1.52 - 1.83	 	 -		 	 	 	100	99	90	61	40	31	╁─
MS-T-3	B-1	0.5 - 2.0	0.15 - 0.61	 		 			 	 	<u> </u>	100	99	97	94	11
	b-2	7.0 - 8.0	2.13 - 2.44				1					100	96	77	59	
	b-3	12.0 - 13.0	3.66 - 3.96						100	91	83	61	24	13	10	\Box
MS-T-5	B-1	0.5 - 2.0	0.15 - 0.61	 	 -	 	 	100	87	77	67	53	23	11	8	+
			 		 		ļ —									
MS-T-6	B-1	0.5 - 2.0	0,15 - 0,61						100	91	81	71	58	40	30	
	b-2	10.0 -11.0	3.05 - 3.35					100	98	90	79	62	19	9	7	<u> </u>
MS-T-7	B-1	0.5 - 2.0	0.15 - 0.61	 	 	 	100	92	81	62	44	33	23	17	14	+
MS-T-8	B-1	0.5 - 2.0	0.15 - 0.61	-		ļ	100	95	73	66	57	49	40	34	31	+-
MS-P-2	b-1	0.5 - 2.0	0.15 - 0.61													上
MS-P-4	b-1	0.5 - 2.0	0.15 - 0.61					100	92	85	72	49	15	6	5	+-
11101-4		0.0 - 2.0	0.70 - 0.07	1		 	-	100	52	- 60		1 73	1.5		Ť	土
MS-P-7	ь1	0.5 - 2.0	0.15 - 0.61							100	99	97	85	69	58	Ŧ
MS-P-9	B-1	0.5 - 2.0	0.15 - 0.61	╂			100	90	68	56	40	28	18	11	9	+
																I
MS-CS-5	b-1	0.0 - 0.5	0.00 - 0.30				100	85	67	60	54	49	46	42	35	+
MS-CS-12	b-1	0.5 - 2.0	0.15 - 0.61						100	77	62	51	41	35	31	土
140 62 65												1	1	-		T
MS-CS-20	b-1	0.5 - 2.0	0.15 - 0.61		<u></u>	<u></u>	1		<u> </u>	L	l	100	99	92	82	1

NOTES:

(a) Sample types

(c) USCS - Unified Soil Classification System

SS - Standard split spoon

P - Pitcher

(d) * Indicates that test has been performed

0 - Fugro Orive

and results are included in this report

B,b - Buik

(b) MP - Not Plastic

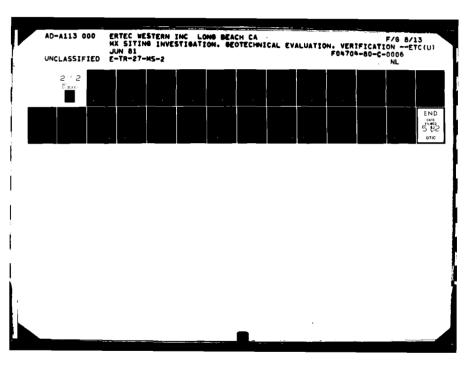
										- 11	N-S I TU			C	OMPACTE			Ð	08
ARD S	IEVE I		PART SIZE LT OR C	(mm)		TERBE Mits (USCS	DRY WEL		NOISTURE Content (5)	SATURATION (\$)		MAXI Dry De	MUM NSITY	OPTIMUM Moisture (\$)	SPECIFIC GRAVITY OF SOLIDS	TRIAXIAL (UNCONFINED COMPRESSION
40	100	200	.005	.001	LL	PL	ΡI	(C)	(pcf)	(kg/m ³)	3 5 5 E	1 2 S	VOID RATIO	(pcf)	(kg/m³)	TON O	SPE GRA OF	TRI	울통
64	37	25		-		<u> </u>	NP	SM	111.3	1783	12.8	67.6	0.51	(77	<u> </u>				
36	19	13				 	 	SM	113.8	1823	11.0	61,7	0.48		<u> </u>				•
57	28	18					NP	SM	106,3	1703	11.3	51.9	0.59						
38	18	12						SW-SM	108.0	1730	11.9	57.1	0.56						
								SM	91.7	1469	15.3	49.3	0.84						
								SM	92.9	1488	4.2	13,8	0.81					•	<u> </u>
								SM	88.4	1416	13,5	40.2	0.91					٠	
88	62	40	11	6			NP	SM	93,6	1499	13.0	43.8	0.80					•	
69	42	26	L				<u> </u>	SM	111.7	1789	8,4	44.8	0,51			L			<u> </u>
	<u> </u>	ļ	 				NP	SW-SM	106,7	1709	16.2	75.4	0.58						ι
30	14	10		igsqcut	L			SW-SM	105,2	1685	15.6	70.1	0.60	L	L			L	}
-	01	70				-	⊢ .	<u> </u>		<u> </u>	 		-	444.0	4000	1	0.00		}
89	81	72			25_	21	4	CL-ML		<u> </u>	<u> </u>	<u> </u>	_	114.0	1826	15.0	2.68		}
CE	20	-				40		<u> </u>			 -				 	 			
65	39 40	31			30	16	14	SC		<u> </u>	ļ	}	 		 	}			├
61	40_	31				├	NP	SM			ļ ——		 			 		<u> </u>	
99	97	94	17	7	31	20	1.				 		├		 	 	<u> </u>	—	╂~~~
96	77	59		'	31	20	NP	CL ML		 			┼			┼──	 		+
24	13	10			_		INF	SW-SM		 -			├		 	┼		-	(
=-		H					├	344-3141					 	 	 	 	 	├─	+
23	11	8				 		SW-SM			 -		┼─	126.0	2018	9.4	 	-	
		- •				├──	 	344-344		 	 		┼─	1200	120.0	+ -:-	 		†
58	40	30				 	\vdash	SM		 -	}	 -	┼──	 -	 	+	 	 	
19	9	7				┢──	 	SW-SM			\vdash		 		 	+	 	 -	 -
	<u> </u>					 	f	0			 		┼──		┼──	+			†
23	17	14		_		<u> </u>		GM			 		\vdash	131.5	2106	9,0	2.66		
\exists								<u> </u>				 	┼──	13113	1	†			
40	34	31			32	21	11	GC		<u> </u>		t	t	119.0	1906	12.5			T
													 						
\Box							NP	ML					1						
\Box																			L
15	6	5					L	SW-SM									<u> </u>	L	↓
					L		L			L					<u> </u>		 		
35	69	58					NP	ML		L				L	<u> </u>	<u> </u>	↓	└	↓
										<u> </u>	<u> </u>	L			<u> </u>	 _	<u> </u>	<u> </u>	↓
18	11	9					L	GP-GM			<u> </u>	<u> </u>		L		<u> </u>		<u> </u>	↓
							<u> </u>							L		↓		 -	↓
16	42	35			33	21	12	GC		ļ	 _	<u> </u>	<u> </u>	<u> </u>	↓	 	 	 -	+-
							\sqcup			<u> </u>	L		<u> </u>	<u> </u>		↓	├	↓	<u> </u>
11	35	31			\Box		lacksquare	GM		L		L	 		↓	↓			+
. 					Щ.	<u> </u>		<u> </u>	ļ	<u> </u>	 	ļ	 	 _	↓	 		₩	+
9	92	82	1	-				NP		NP ML									

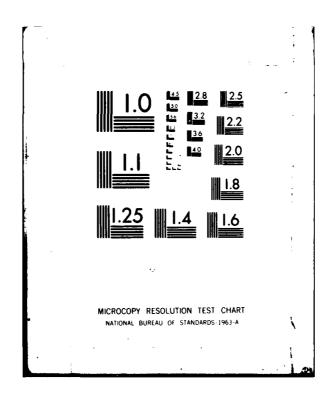


SUMMARY OF MULESHO

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Щ		OMPACTE	0		9	_ =		8		
RATIO	MAX Dry De	MSITY	711806 11570rg (\$)	SPECIFIC GRAVITY OF SOLIDS	TRIAXIAL (4)	UNCONFINED COMPRESSION	DIRECT Shear	CONSOLIDATIO	CHEMICAL	e .
	(pcf)	(kg/m ³)	2 =	2 2 2	1	35	32	3	5	85
.51										
.48						•			•	
.59										
.56 .84										
.81		 	├	 		 -				├
.91		 -	 		÷					
.80			\vdash	-	+					
.51		t			 -					$\vdash \vdash \vdash$
.58										
.60									•	
\vdash	114,0	4000								
	114.0	1826	15.0	2,68						
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	126.0	2018	 	 		 	 			
	120.0	2010	9.4	 	├	├	 -			├┷┤
		 	 	 		├				$\vdash \vdash \vdash$
_		 	 	 		 			 	
	131,5	2106	9,0	2.66						·
						<u> </u>	<u> </u>			
	119.0	1906	12.5	L		↓		ļ		
		}		 		├			-	-
			 	 		 		 	 	
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SUMMARY OF LABORATORY RESULTS MULESHOE VALLEY, NEVADA PAGE 2 OF 2

30 JUN 81

TABLE BO

								 	 		 	 	 	 ,
SURE	kN/m²	0	0	0	0	0	0							
BACK	ks í	0	0	0	0	0	0							
STRAIN	$\mathbf{\mathcal{L}}$	0.04	0.04	20.0	0.02	0.02	0.01							
NAXIMUM DEVIATOR STRESS (0, -0)	kN/m²	480	744	1018	1190	1709	2117			-				
MAX OFVI STRESS	ks f	10.0	15.5	21.2	24.8	35.6	44.1							
NING RE(O ₃)	kN/m ²	144	216	288	288	432	675							
PRESSURE (03)	ks t	3.0	4.5	6.0	6.0	9.0	12.0							
MOISTURE	(%)	10.5	12.4	10.0	4.2	13.0	13.5							
DENSITY	kg/m ³	1663	1660	1709	1488	1499	1416							
DRY D	pc (103.8	103.6	106.7	92.9	93.6	88.4				}			
TYPE OF	TEST	aэ	аэ	aэ	аэ	аэ	aэ							
1108	TYPE	SM	SM	SM	SM	SM	SM		1					
INTERVAL	METERS	9.51 - 9.66	9.30 - 9.45	9.72 - 9.88	18.35 - 18.50	18.84 - 18.99	18.59 - 18.75							
SAMPLE	FEET	31.2 - 31.7	30.5 - 31.0	31.9 - 32.4	60.2 - 60.7	61.8 - 62.3	61.0 - 61.5							
SAMPLE	36 .	P-8	P-8	8-d	P-12	P-12	P-12							
BORING	MU.	MS-B-1			MS-B-3									



SUMMARY OF TRIAXIAL COMPRESSION
TEST RESULTS
MULESHOE VALLEY, NEVADA

30 JUN 81

TABLE 12-2

		_		_	,	,	_	_	_	_	,	,	_	_	_	_	_	_	_	_	_	_	,	_	_	_	_	_	
HE I GHT/	DIAMETER	2.09	2.00			1		ļ ļ																					
DEGREE OF	(\$)	22.2	61.7																										
MOISTURE	(\$)	10.7	11.0																										
i .	k 8 / m 3		1823																										
DRY DENSITY	pot	72.6	113.8																										
IF I NED TRENGTH	kN/m2	118	92																										
UNCONFINED Comp. Strength	ks f	2.5	1.9																										
7108	_	CL	SM																										
NTERVAL	METERS	0.49 - 0.73	9.20 - 9.36																										
SAMPLE INTERVAL	FEET	1.6 · 2.4	30.2 - 30.7																										
SAMPLE		p.1	0-9																		• 								
BORING SAMPLE	10.	MS-B-1	MS-B-3																										



SUMMARY OF UNCONFINED COMPRESSION TEST RESULTS MULESHOE VALLEY, NEVADA

30 JUN 81.

TABLE 11-9-3

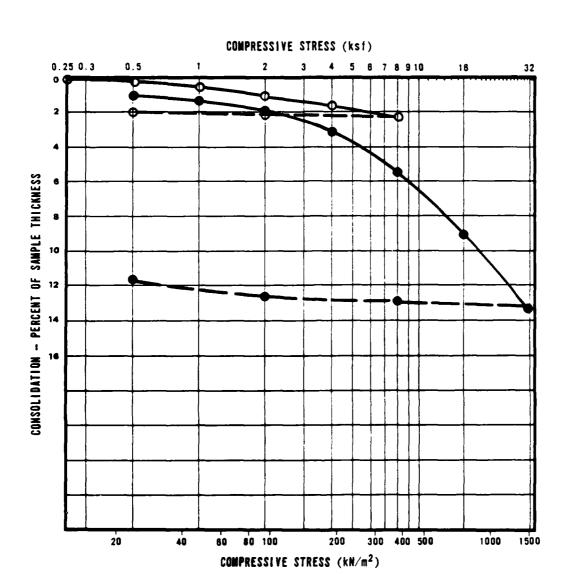
	SAMPLE	SAMPLE 11	NTERVAL	SOIL	NORMAL	STRESS	MAX SHEAR	MUM Strength
NO.	NO.	FEET	METERS	TYPE	ksf	kN/m²	ksf	kN/m 2
MS-B-1	D-5	15.5 - 16.0	4.72 - 4.88	SM	1.5	72	1.80	86
		·			2.3	108	2.43	116
			-		3.0	144	2.98	143
MS-B-3	D-7	21.0 - 21.5	6.40 - 6.55	SP-SM	2.0	96	2.56	123
			-		3.0	144	3.26	156
					4.0	192	4.91	235
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SUMMARY OF DIRECT SHEAR TEST RESULTS MULESHOE VALLEY, NEVADA

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.TABLE 11-9-4



SYMBOL	BORING NO.	SAMPLE NO.	SAMPLE	INTERVAL	SOIL		TIAL	INITIAL MOISTURE CONTENT	INITIAL VOID RATIO	INITIAL DEGREE OF SATURATION
			FEET	METERS	1	pcf	kg/m3	(%)	RALIU	(%)
0	MS-B-2	D-6	15.5 - 16.0	4.72 - 4.88	ML	91.8	1471	8.8	0.84	28.4
					i					

O AT FIELD MOISTURE

AFTER ADDITION OF WATER

____ COMPRESSION

- - - REBOUND



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CONSOLIDATION TEST RESULTS MULESHOE VALLEY, NEVADA

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FIGURE 11-9-1

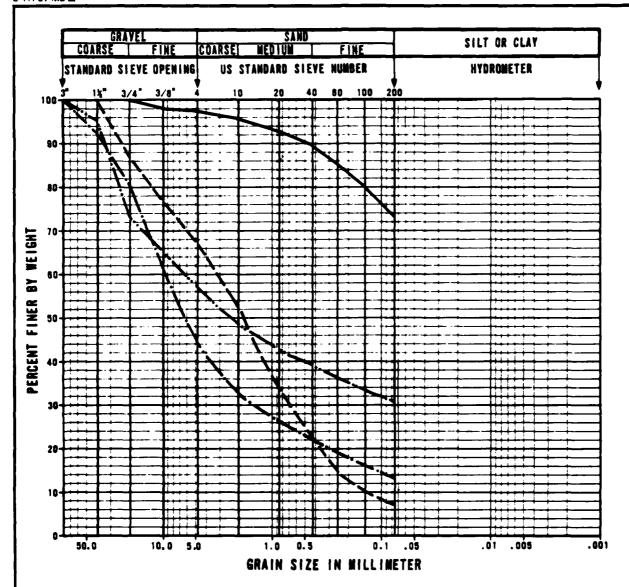
FERS TYPE MR/Kg Mg/kg Mg	TIVITY	KAMPIF		SAMPLE INTERVAL				3	WATER SOLUBLE	<u></u>	CALCTUR
P-6 200-20.9 6.10-6.37 SM 8.2 42 21 2 53 D-3 55-6.0 1.68-1.83 SM 8.0 76 10 3 61 D-9 30.2-30.7 9.20-9.36 SM 84 20 70 4 81 P-15 988-99.8 30.11-30.42 SW-SM 84 21 <6 <1 118 P-1 0.5-2.0 0.15-0.61 ML 8.0 3 5 <1 149 P-1 0.5-2.0 0.15-0.61 ML 8.0 3 5 <1 149 P-1 0.5-2.0 0.15-0.61 ML 8.0 3 5 <1 149 P-1 0.5-2.0 0.15-0.61 ML 8.0 3 5 <1 149 P-1 0.5-2.0 0.15-0.61 ML 8.0 3 5 <1 149 P-1 0.5-2.0 0.15-0.61 ML 8.0	9	8			TYPE	푎	SODIUM	CHLORIDE	SULPHATE	CALCIUM	CARBONATE
P-6 20.0-20.9 6.10-6.37 SM 8.2 42 21 2 5.5 D-3 55-6.0 1.68-1.83 SM 84 20 70 4 81 D-9 30.2-30.7 9.20-9.36 SM 84 20 70 4 81 P-15 36.8-96.8 30.11-30.42 SW-SM 8.4 21 <6 <1 118 P-1 0.5-2.0 0.15-0.61 ML 80 3 5 <1 149 P-1 0.5-2.0 0.15-0.61 ML 80 3 5 <1 149 P-1 0.5-2.0 0.15-0.61 ML 80 3 5 <1 149 P-1 0.5-2.0 0.15-0.61 ML 80 3 5 <1 149 P-1 0.5-2.0 0.15-0.61 ML 80 3 5 <1 149 P-1 0.5-2.0 0.15-0.61 ML 80 3 5 <1 149 P-1 0.5-2.0 0.15-0.61 ML 80 3 6 <1 149 P-1 0.5-2.0 0.15-0.61 ML 80 3 6 <1	1		ĺ	METERS			mg/kg	mg/kg	mg/kg	mg/kg	mo/ko
D-3 5.5.6.0 1.68-1.83 SM 9.0 76 10 3 61 D-9 30.2-30.7 9.20-9.36 SM 8.4 20 70 4 81 P-15 986.8-98.8 30.11-30.42 SW-SM 8.4 21 <66 <1 118 b-1 0.5-2.0 0.15-0.61 ML 8.0 3 5 <1 149	S-8-1	P-6	20.0 - 20.9	6.10 - 6.37	SM	8.2	42	21	2	53	Ē
D9 30.2 · 30.7 9.20 · 9.36 SM 8.4 20 70 4 81 P·15 98.8 · 99.8 30.11 · 30.42 SW·SM 8.4 21 <6	S-B-2	D-3	5.5 - 6.0	1.68 - 1.83	S S	9.0	9/	01	ဧ	61	158
P-15 98.8 9.9.8 30.11 - 30.42 SW-SM 8.4 21 <6 <1 118	S-8-3	6 -0	30.2 - 30.7	9.20 - 9.36	SM	4.8	20	82	4	81	317
b-1 0.5-2.0 0.15-0.61 ML 8.0 3 5 <1 149	S-8-3	P-15	86.8 - 99.8	30.11 - 30.42	SW-SM	8.4	21	9 >	7	118	081
	S-P-2	þ-1	0.5 - 2.0	0.15 - 0.61	¥	8.0	3	2	7	149	503
	1										
						_					



SUMMARY OF CHEMICAL TEST RESULTS MULESHOE VALLEY, NEVADA

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TABLE 12-0-6



SYMBOL	COMPOSITE Sample	ACTIVITY	SAMPLE	INTERVAL	SOIL
21 MDOF	NUMBER	NUMBER	FEET	METERS	TYPE
	A	MS-T-1	0.5 · 2.0	0.15 - 0.61	CL·ML
	В	MS-T-5	0.5 · 2.0	0.15 - 0.61	SW-SM
	С	MS-T-7	0.5 - 2.0	0.15 - 0.61	GM
			0.5 - 2.0	0.15 - 0.61	GC
	g D	MS-T-8 -			⊣ GC

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GRAIN SIZE CURVES, CBR TESTS MULESHOE VALLEY, NEVADA

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FIGURE II-0-2

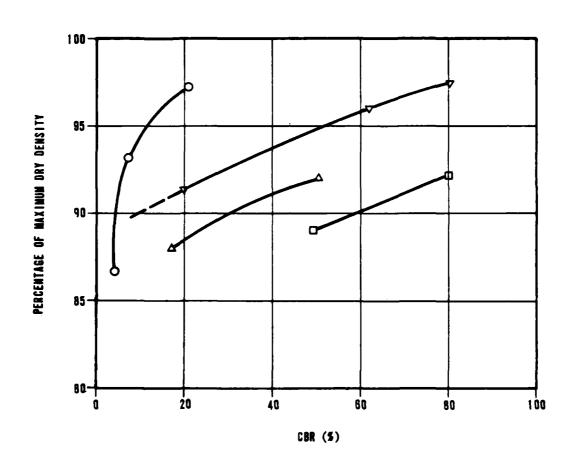
A CL-ML 72 A SW-SM 8	200	=	Ī	2002000		DE DEMO		DRY DENSITY	ENSITY	MOISTURE		500
CL-ML	7		P.	GKAVIIT	pc f	kg /m3	(%)	pcf	kg/m3	(%)	DRY DENSITY	(%)
CL-ML	5							110.9	1111	15.1	67.3	21
CL-ML SW-SM	7							106.3	1703	15.1	93.3	7
SW-SM		52	4	2.68	114.0	1826	15.0	8.86	1582	15.2	2'98	4
SW-SM												
SW-SM	٦											
SW-SM								116.3	1863	9.3	92.3	80
WS-WS		-						112.1	1796	9.1	0.68	49
					126.0	2018	9.4					
								121.2	1942	9.1	92.2	51
		<u>, </u>						115.8	1855	8.5	88.1	17
C GM	4			2.66	131.5	2106	0.6					
			_									
								116.1	1859	14.6	97.5	80
								114.3	1831	13.7	0.96	61
D GC 31	<u> </u>	32	=		119.0	1906	12.5	108.6	1740	12.3	91.3	21
							·					



CALIFORNIA BEARING RATIO (CBR) TEST RESULTS MULESHOE VALLEY, NEVADA

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TABLE 200



SYMBOL	COMPOSITE SAMPLE NUMBER	SOIL
Α	0	CL-ML
В	0	SW-SM
С	Δ	GM
a	▽	GC



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CALIFORNIA BEARING RATIO (CBR) CURVES MULESHOE VALLEY, NEVADA

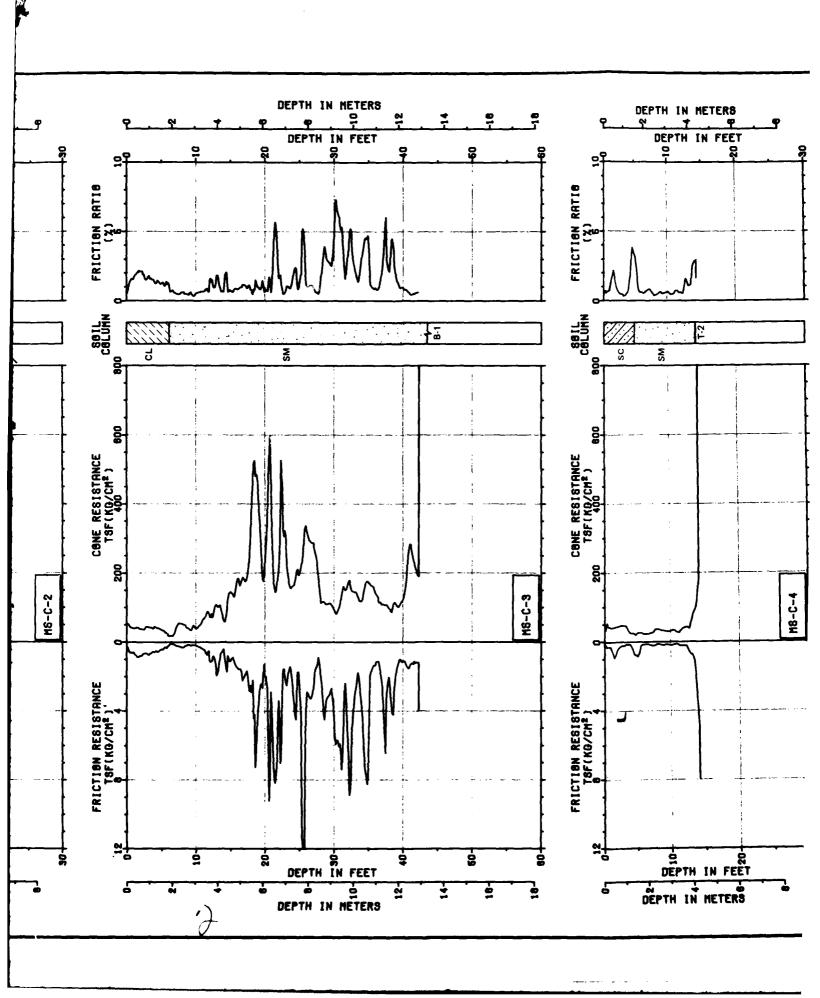
30 JUN 81

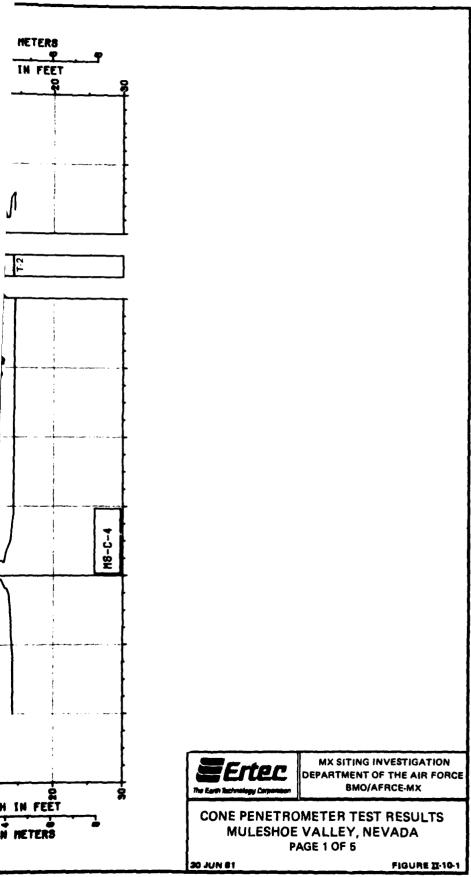
FIGURE II-0-3

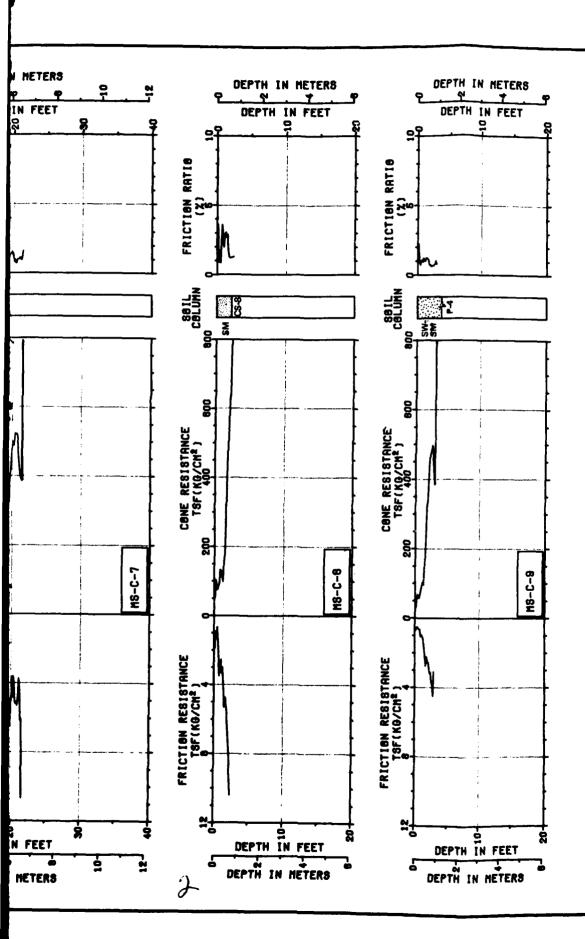
10.0 CONE PENETROMETER TEST RESULTS

<u>Explanation</u>: The results of all cone penetrometer tests are presented in this section. Explanations of the test results are as follows:

- A. Depth Corresponds to depth below ground surface.
- B. Friction Resistance The resistance to penetration developed by the friction sleeve, equal to the vertical force applied to the sleeve divided by its surface area. This resistance is the sum of friction and adhesion.
- C. Cone Resistance The resistance to penetration developed by the cone, equal to the vertical force applied to the cone divided by its horizontally projected area.
- D. Friction Ratio The ratio of friction resistance to cone resistance.
- E. Designation Each cone penetrometer test is identified by a number: for example C-1.
 - C abbreviation for the CPT
 - 1 number of the test
- F. Soil Column A graphical presentation of the soil type versus depth at each cone penetrometer test location. The Unified Soil Classification Symbol (Table II-6-1) for each different soil type is listed immediately to the left of the soil column. Immediately below the soil column, the activity number for the corresponding boring, trench, test pit, or surficial soil sample at each CPT location is given.





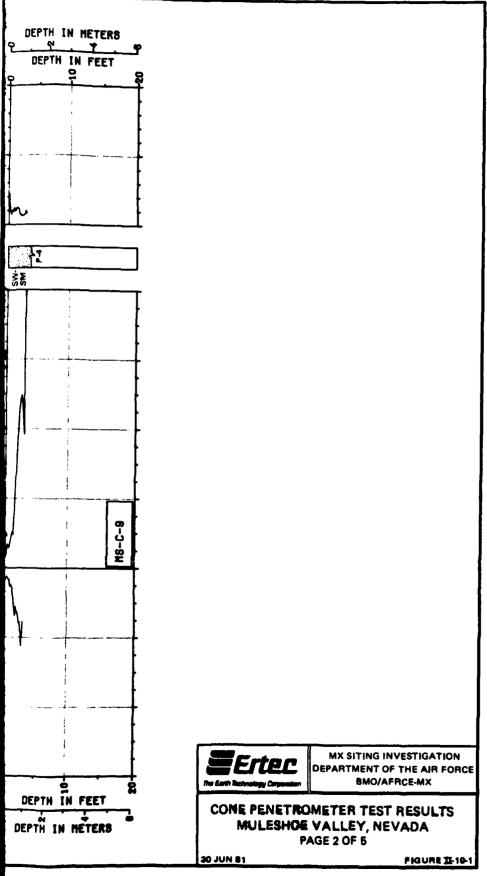




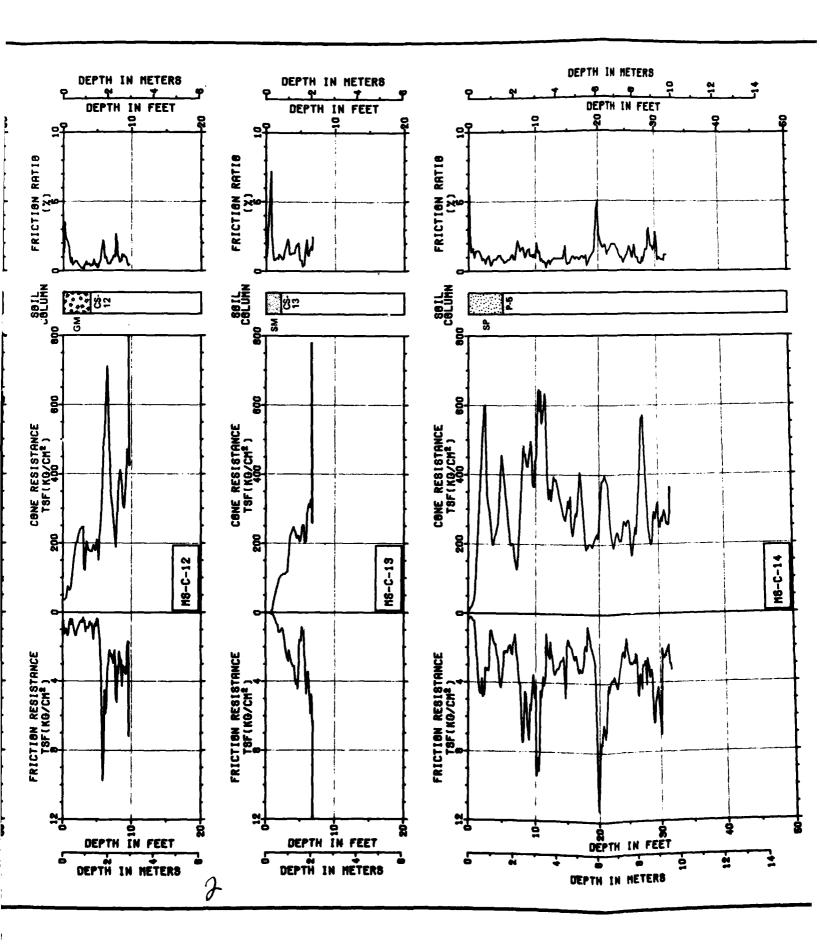
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CONE PENETROMETER TEST I MULESHOE VALLEY, NEV PAGE 2 OF 5

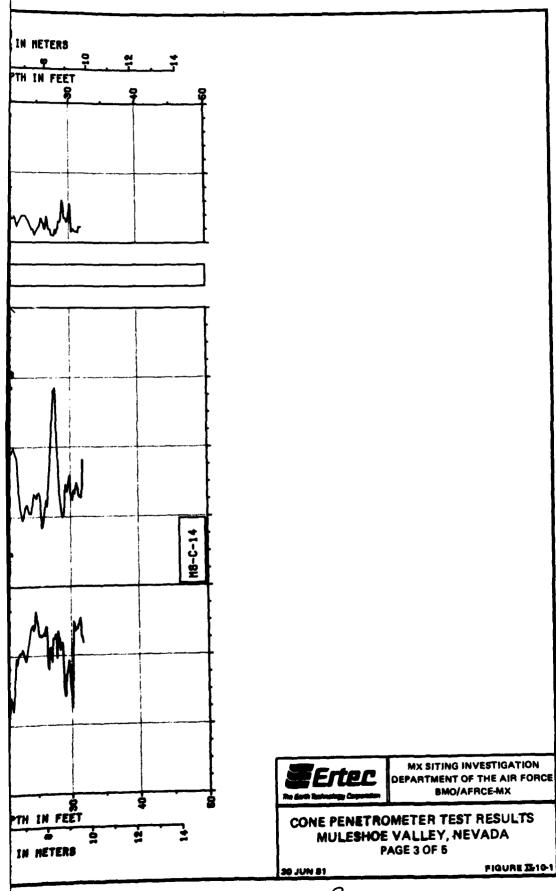
30 JUN 81

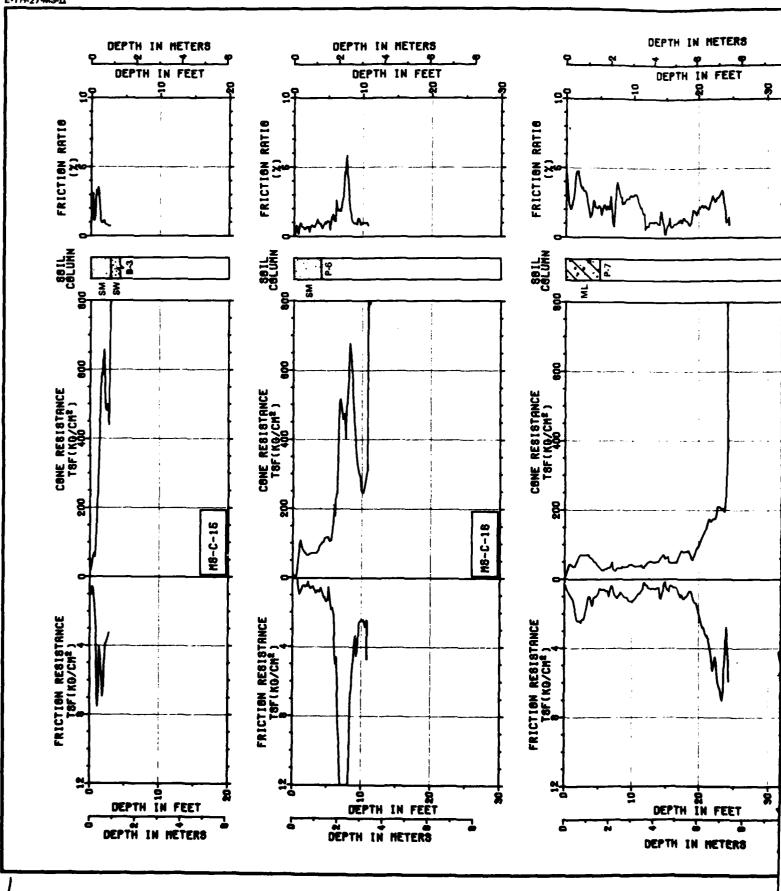


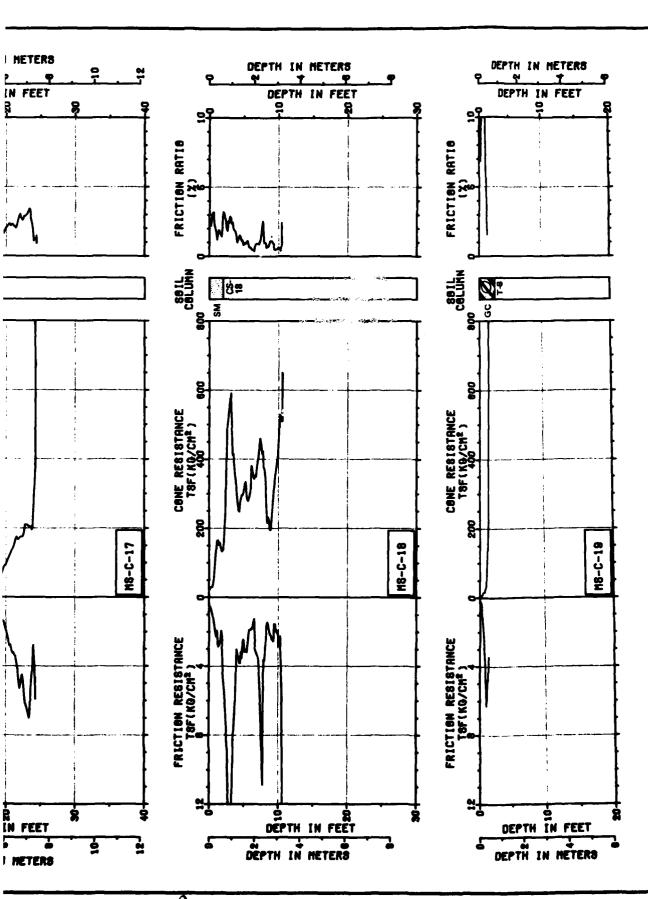
DEPTH IN METERS







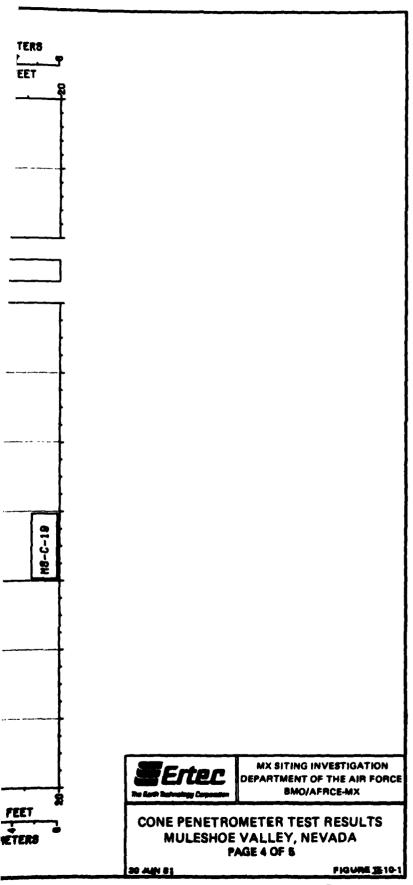


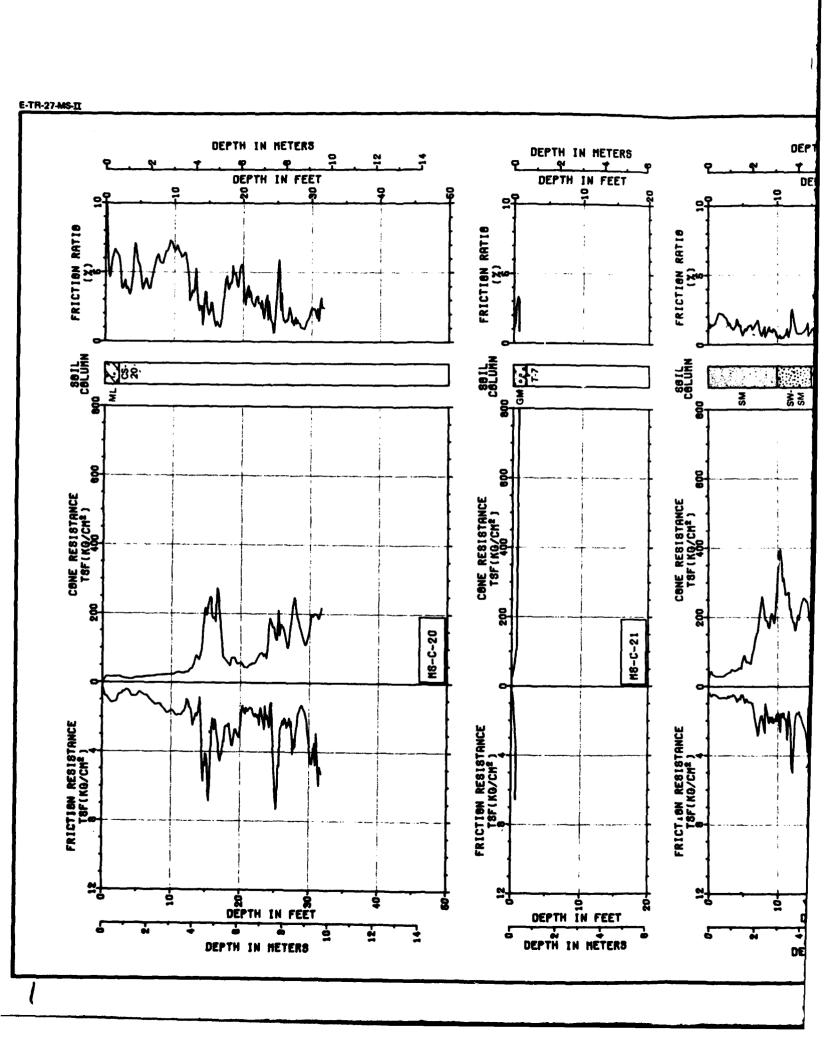


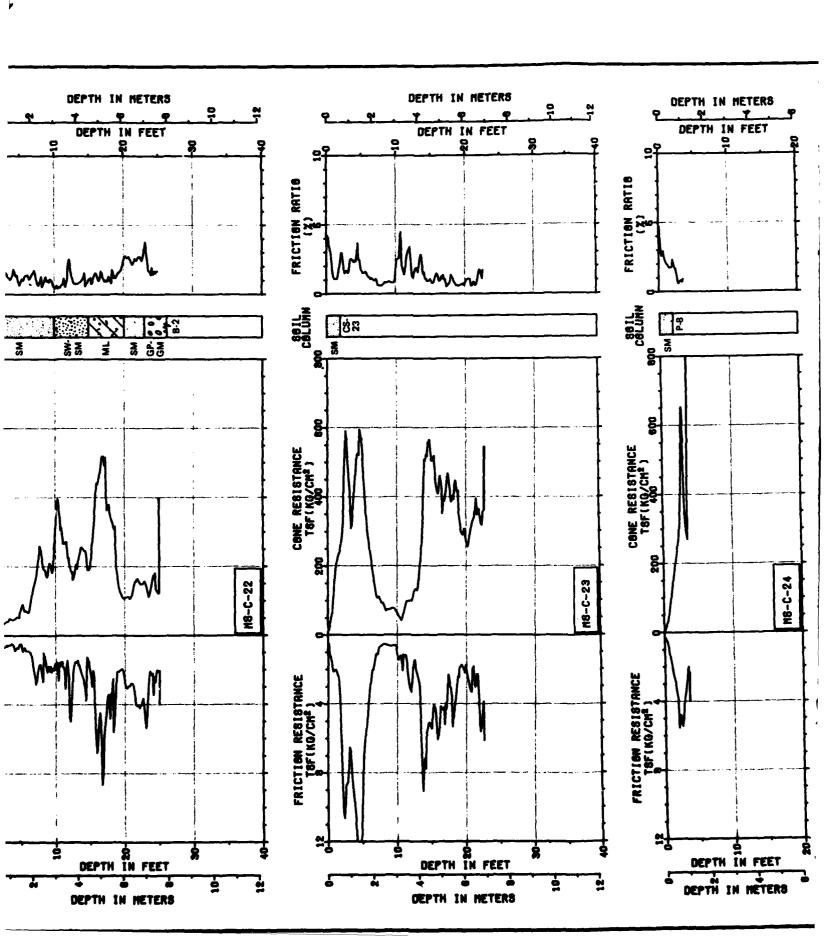


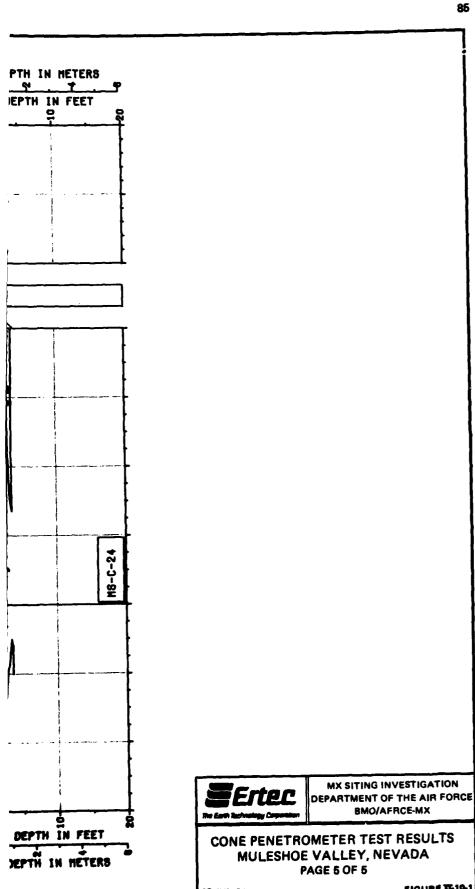
CONE PENETROME MULESHOE VA PAGE

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FIGURE IE-10-1

END

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